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Development of a Railway Out-of-gauge Freight Transport Routing Optimal Method

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Abstract: Railway out-of-gauge freight (ROF) is beyond railway gauges in its dimensions, which could be risks leading to serious railway accidents. This article presents a new methodology to search for a safest and more economic route of ROF by taking safety and cost objectives into consideration. In this method, a mathematical model is proposed based on the transport costs as optimization objectives with the constraints of flow balance and safety gap clearance in which ROF transport routing generation, loading outline and railway gauge double-checking algorithms are established, and then a ROF transport routing model combining transportation costs, loading outlines and railway gauges are developed. The proposed method can be used to determine the safest and more economic ROF route. A case study is used to demonstrate the application of the proposed method.

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1. Introduction

Railways is by far the safest form of ground transportation. However, the railway now finds itself in a situation where safety is a real issue that has to be dealt with in a new public culture of rapid change, short-term pressures and instant communications [1, 2, 3]. Railway out-of-gauge freight (ROF) refers to those oversized cargoes that are wider or longer or higher. In other words, the loading outlines are beyond rolling stock gauges such as platforms, tunnels and signal equipment, which require safe gaps and clearances between trains and infrastructures [4, 5]. A rolling stock gauge defines the

29 maximum profile dimension of a train, i.e., a minimum gap is required between ROF loading outline
30 and rolling stock [6, 7]. Sufficient clearances between ROF loading outlines and railway gauges are
31 usually called as safety gaps. However, loading outlines of a ROF train are often beyond the rolling
32 stock gauges along with its route [7]. Therefore, railway operators have to check safety clearances in
33 the railway network to ensure the safest route to be selected for a ROF train [8].

34 Wilson [4] reviewed the UK railway network and emphasized that ROF trains with oversized
35 loading outlines particularly affect safety of the UK rail network. Chen *et al.* [9] proposed a vehicle-
36 road reliability and safety simulation model that can be used to simulate a safe transportation of out-
37 of-gauge goods trains using Simpack simulation software. Lei *et al.* [10] developed an object-oriented
38 method for calculating out-of-gauge goods outline, which addresses object description, projection, and
39 integration. Perez *et al.* [5] developed a sophisticated gauging method to measure railway
40 infrastructure gauges. Chen *et al.* [15] proposed an optimal model for the selection of ROF
41 transportation route. Luo *et al.* [16] developed a reconstruction model for route planning of multimodal
42 transportation of oversize and heavyweight cargo, and such a model focuses on loading outlines and
43 weights of trains. However, these studies only focus on railway freight train design, routing and
44 scheduling problems, but do not address ROF problem, for example, safety gap distance checking,
45 which have potential risks leading to accidents [11, 12, 13] such as train collision with infrastructure
46 along the route causing train derailments.

47 A ROF train is different from common railway freight train. When a train is marshaled with rail
48 cars loaded ROF goods, the train turns to an out-of-gauge one. Therefore, the risks leading to accidents
49 of ROF trains are higher than common railway freight trains, which strict operation requirements for
50 the ROF trains are required to ensure safe transportations, for example, speed control and safety gap
51 limit are required [6, 14]. The safe transportation of a ROF train greatly depends on the gap distances
52 between ROF loading outlines and railway gauges along its route from its original station to destination
53 station. Furthermore, there will be a large amount of data that the ROF routing problems cannot be
54 solved quickly by using current methods in a simple and accurate way because the data of railway
55 gauges are always changed in real time across railway network according to current actual situations.
56 It is necessary to develop new methods for safety calculating and checking by taking current actual
57 railway gauge situations into consideration. Literature search shows that no research has proposed
58 railway gauge double-checking method to ensure a safe ROF transportation that can be selected.
59 Literature search also shows that no research addresses economic issue when planning a ROF route.
60 Therefore, selection of a ROF route may also need to take costs into consideration in the decision-
61 making process so that a safe and economic ROF transportation route can be determined.

62 This paper presents a new methodology for the selection of a safe and economic ROF route in the
63 railway network which will provide a method and tool to railway operators in the planning of the safe
64 and economic routes for ROFs. In this method, case-based reasoning k -shortest path algorithm is
65 employed to generate possible alternative ROF routes. The proposed double-checking approach is then
66 proposed and applied to check safety gaps and clearances, and finally transportation costs are taken
67 into consideration in the decision-making process to ensure that a safe and economic ROF route can
68 be selected. By using the proposed method, a safe and economic route for a ROF train from its original
69 station to destination station in the railway network can be determined in which the flow balance at
70 each railway station, safe clearances between ROF loading outlines and railway gauges along its route
71 are taken into consideration. The significant contributions of this study can be summarized as follows:

- 72 • Possible ROF route generation method has been established to take historical data, current ROF
73 loading outlines and existing railway gauges into consideration,
- 74 • Double-checking approach has been developed to check railway gauges, safety gap clearances
75 and operation conditions along the possible routes to guarantee a safe ROF transportation,
- 76 • A ROF route optimal model has been developed by taking safety and economics in the decision-
77 making process so that a ROF safe and economic transportation route can be determined,
- 78 • The proposed method provides a great opportunity to incorporate it into expert systems in the
79 railway industry to enhance the safe and economic operations for railway transportation.

80 The remainder of this paper is organized as follows: After Introduction Section, Section 2
81 describes the analysis of the flow balance and safety gap constraints between ROF loading outlines
82 and railway gauges. Section 3 discusses cost estimation based on distances, out-of-gauge grades and
83 extra transport costs, and objective functions are established. The proposed ROF route optimal model
84 is presented in Section 4. A ROF safe and economic transportation route decision support process is
85 presented in Section 5 in which ROF loading outlines and railway gauges double-checking algorithm
86 and a solution process based on safety requirements are described. A case study is used to demonstrate
87 the performance of the proposed methodology is presented in Section 6. Finally, conclusions are given
88 in Section 7.

89

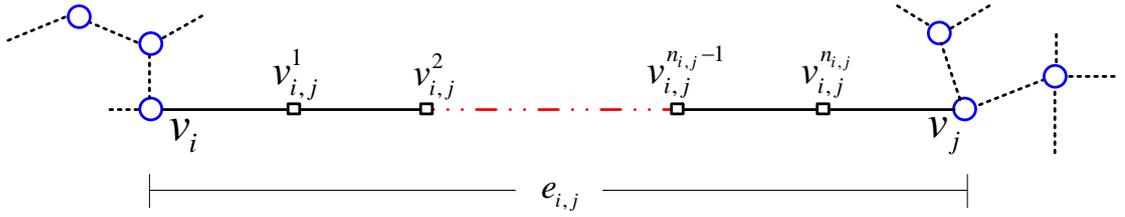
90 **2. Flow Balance and Safety Gap Clearance Constraints**

91 The selection of a ROF transport route usually depends on ROF loading outlines and rolling

92 stock gauges in the railway network. The following assumptions are currently applied to reduce the
 93 problem complexity: (i) ROF loading outline is based on ROF loading method as planned, (ii) railway
 94 infrastructures satisfy ROF requirements, e.g., bridges along the route are strong enough to support
 95 ROF vehicle weights, and (iii) railway gauges are unchangeable, for example, station platforms, signal
 96 towers, and tunnels are not changed.
 97

98 2.1 Flow balance constraints

99 There are many stations in a railway network, which can be classified as key stations and
 100 intermediate stations. Intermediate stations are within the railway network between two adjacent key
 101 stations. Fig. 1 shows a typical a route.
 102



103
 104 **Fig. 1** A typical route

106 In Fig. 1, v_i and v_j denote two key stations, $e_{i,j}$ is the key section between two key stations v_i and
 107 v_j , which are connected by $n_{i,j}$ ($n_{i,j} \in \mathbf{N}$) intermediate stations. Intermediate stations are represented
 108 by $v_{i,j}^k$ ($k = 1, 2, \dots, n_{i,j}$). $v_{i,j}^k$ is the k th intermediate station between v_i and v_j ($v_{i,j}^0 = v_i, v_{i,j}^{n_{i,j}-1} =$
 109 v_j). Suppose key stations n_{key} be identified in the route, $\forall i$ and $\forall j \in \{i \text{ and } j =$
 110 $1, 2, \dots, n_{\text{key}}\}$ (n_{key} is the total number of key stations). Let $\mathbf{G} = (\mathbf{V}, \mathbf{E})$ be a key ROF railway
 111 network in which includes all of key stations, a whole freight network can be expressed as $\mathbf{G}' = (\mathbf{V}', \mathbf{E}')$
 112 where includes all key and intermediate stations. $\mathbf{V} = \{v_i | i = 1, 2, \dots, n_{\text{key}}\}$ denotes the set of all key
 113 stations, $\mathbf{E} = \{e_{i,j} | i, j = 1, 2, \dots, n_{\text{key}}\}$ denotes the set of sections between two key sections, $\mathbf{V}' =$

114 $V \cup V''$ ($V'' = \{v_{i,j}^k | k = 0, \dots, n_{i,j}, e_{i,j} \in E\}$) denotes the set of all intermediate stations between v_i
115 and v_j , and V'' represents all intermediate stations except key stations, $E' =$
116 $\{v_i v_{i,j}^1, \dots, v_{i,j}^{k-1} v_{i,j}^k, \dots, v_{i,j}^{n_{i,j}} v_j | e_{i,j} \in E, n_{i,j} > 1\} \cup \{v_i v_{i,j}^1, v_{i,j}^1 v_j | e_{i,j} \in E, n_{i,j} = 1\} \cup \{v_i v_j | e_{i,j} \in$
117 $E, n_{i,j} = 0\}$ denotes the set of all intersections from key station v_i to key station v_j . For example,
118 original and destination stations in a railway network are usually two key stations, i.e., $v_o, v_d \in V$, a
119 safe transport route from original station v_o to destination station v_d can be determined directly by
120 the key ROF railway network G , and the whole freight network G' .

121 Suppose ROF flow balance is in the key ROF railway network G , and a ROF train flow-out at the
122 original station v_o and flow-in at the destination station v_d , which is equivalent to ROF flow-in and
123 flow-out at other railway stations along a ROF route. The key ROF railway network G is regarded as
124 a direction map that a key station receives ROF flow from v_i called as an out-adjacent key station to
125 next key station v_j called as in-adjacent key station. Let $\varphi(v_i) = \{v_j \in V | e_{i,j} \in E\}$ ($v_i \{i =$
126 $1, 2, \dots, n_{key}\}$) be the out-adjacent key station set, and $\beta(v_i) = \{v_j \in V | e_{j,i} \in E\}$ ($v_i \{i =$
127 $1, 2, \dots, n_{key}\}$) be the in-adjacent key station set, the flow balance constraint in key railway network
128 G about a ROF transport route can be obtained by

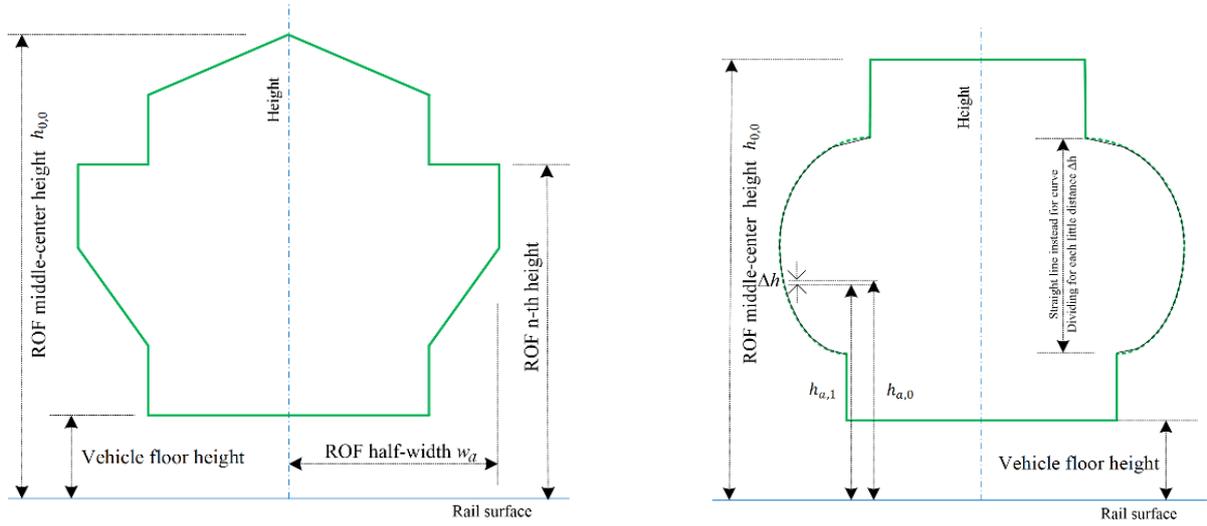
$$130 \quad \sum_{v_j \in \varphi(v_i)} x_{i,j} - \sum_{v_j \in \beta(v_i)} x_{i,j} = \begin{cases} 1 & v_i = v_o \\ 0 & v_i \neq v_o, v_d \\ -1 & v_i = v_d \end{cases} \quad (1)$$

131
132 where $x_{i,j}$ is the decision parameter for a ROF transport route and its value is 0 or 1. For example, if
133 the ROF train visits stations v_i and v_j (v_i and $v_j \in V$), i.e., the key section $e_{i,j}$ is a ROF route, then
134 $x_{i,j} = 1$; otherwise, $x_{i,j} = 0$, i.e., the ROF train does not visit stations v_i and v_j , and $e_{i,j}$ is not a
135 ROF route.

137 2.2 Safety gap clearance constraints between ROF loading outlines and railway gauges

138 ROF loading outlines and railway gauges need to be considered in the selection process of a ROF route

139 process to choose a safe ROF route. Fig. 2 shows typical loading outlines in which include the shaped
 140 ROF loading outline as shown in Fig. 2(a) and the non-shaped ROF loading outline as shown in Fig.
 141 2(b).



143 (a) Shaped ROF loading outline

144 (b) Non-shaped ROF loading outline

145 **Fig.2** ROF loading outlines

146 As can be seen in Fig. 2 (a), the highest height of the ROF loading outline is at the middle-center
 147 point and the lowest height is from rail surface to vehicle floor. Other heights of the ROF loading
 148 outline compared with the middle-center height are called as the 1st-side height, the 2nd-side height, ...,
 149 the n^{th} -side height in a particular order from higher to lower, respectively. If a ROF loading outline is
 150 the non-shaped outline as shown in Fig.2 (b), a Δh can be applied to determine the highest height of
 151 a ROF outline, which $\Delta h=10$ mm is usually used to calculate the outline height. ROF loading outlines
 152 can be usually recorded as shown in Table 1.

153 **Table 1** ROF loading outlines

No.	Location	Higher height/mm	Lower height/mm	Half-width/mm
0	Middle-center height	> Floor height		> 0
1	1 st -side height	> Floor height		> 0
2	2 nd -side height	> Floor height		> 0
...		
n	n^{th} -side height	> Floor height	Floor height	> 0

154

155 Therefore, ROF loading outline can be presented by

156

$$\mathbf{H} = \begin{pmatrix} h_{0,0} & h_{0,1} & w_0 \\ h_{1,0} & h_{1,1} & w_1 \\ \vdots & \vdots & \vdots \\ h_{a,0} & h_{a,1} & w_a \\ \vdots & \vdots & \vdots \\ h_{n,0} & h_{n,1} & w_n \end{pmatrix} \cup \begin{pmatrix} h_{0,0} & h_{0,1} & -w_0 \\ h_{1,0} & h_{1,1} & -w_1 \\ \vdots & \vdots & \vdots \\ h_{a,0} & h_{a,1} & -w_a \\ \vdots & \vdots & \vdots \\ h_{n,0} & h_{n,1} & -w_n \end{pmatrix} \quad (2)$$

158

159 where $h_{a,0} > 0$ and $h_{a,1} > 0$, $h_{a,0}$ is the a^{th} side-height ($a = 0,1, \dots, n$) and $h_{a,1} = h_{a,0} - \Delta h$
 160 where the middle-center height is $h_{0,0}$ as shown in Fig. 2(b). It should be noted that $h_{a,1} = NULL$
 161 only when the height of loading outline is consistent at the height of the a^{th} -side height. w_a ($w_a > 0$)
 162 denotes the width at the a^{th} -side height. w_a and $-w_a$ indicate half-width of the ROF outline at the
 163 right and left hands of the longitudinal center line of the rail track as shown in Fig. 2. In this case,
 164 $h_{0,0} > h_{1,0} > h_{2,0} > \dots > h_{n,0} > 0, h_{n,1} > 0$, i.e., $h_{a,0} > h_{a,1}$ and $h_{a,1} \geq h_{a+1,0}$.

165 Safety gap clearances related to railway gauges need to be taken into consideration [4, 8] in the
 166 determination of ROF transport routes. ROF loading outlines must be beyond rolling stock gauges and
 167 do not exceed railway gauges of railway infrastructures such as bridges, tunnels, platforms, electrical
 168 equipment boxes, signal devices and over-head power lines along a ROF route [17, 18]. Therefore, the
 169 maximum train loading outline must be within minimum railway gauges, which can be expressed by
 170

$$\mathbf{S} = \begin{pmatrix} s_{1,0} & s_{1,1} & b'_1 \\ s_{2,0} & s_{2,1} & b'_2 \\ \vdots & \vdots & \vdots \\ s_{c,0} & s_{c,1} & b'_c \\ \vdots & \vdots & \vdots \\ s_{m,0} & s_{m,1} & b'_m \end{pmatrix} \quad (3)$$

172

173 where the heights of railway gauges are divided into m parts, i.e., $c = 1,2 \dots m$, $s_{c,0}$ ($s_{c,0} > 0$) and
 174 $s_{c,1}$ ($s_{c,1} > 0$). When the height of a ROF loading outline is consistent at the height of the b^{th} -side
 175 height, then $s_{c,1} = NULL$. b'_c ($b'_c \neq 0$) represents the highest height $s_{c,0}$ or the lowest height $s_{c,1}$,
 176 i.e., distances from the longitudinal center line of railway track to railway gauges. If a control point of
 177 the minimum railway gauge lies at the right hand of the longitudinal center line, then $b'_c > 0$;
 178 Otherwise, at the left hand of the longitudinal center line, $b'_c < 0$. Let $\mathbf{S}_{i,j}^k$ ($v_{i,j}^{k-1}, v_{i,j}^k \in \mathbf{V}'$) denote the
 179 minimum railway gauge in the railway intersection $e_{i,j}^k$ ($e_{i,j}^k \in \mathbf{E}'$) in the whole freight network \mathbf{G}' , and
 180 δ (mm) be a safety allowance as the clearance constraint, a safety gap between ROF loading outlines

203

$$e_{i,j}^k \in \{v_i v_{i,j}^1, \dots, v_{i,j}^{k-1} v_{i,j}^k, \dots, v_{i,j}^{n_{i,j}} v_j | x_{i,j} = 1, n_{i,j} > 1, k \in \{1, 2, \dots, n_{i,j}\}\}, \{v_i v_{i,j}^1, v_{i,j}^1 v_j | x_{i,j} = 1, n_{i,j} \geq 1\} \text{ or } \{v_i v_j | x_{i,j} = 1, n_{i,j} = 0\} \quad (6)$$

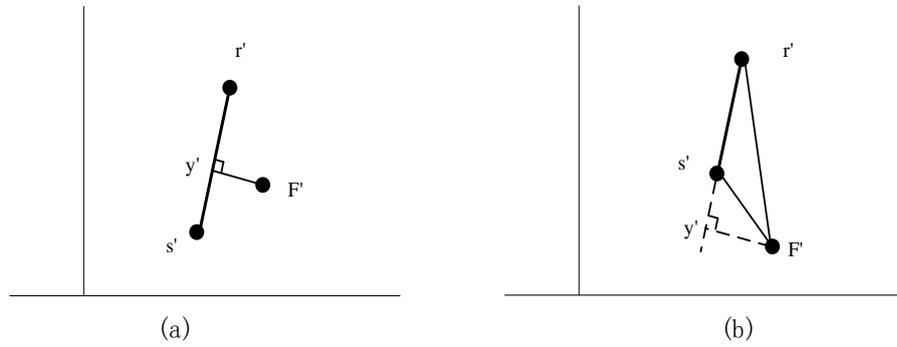
206

207 Therefore, the safety gap clearance constraint Eq. (4) can be rewritten as

208

$$dis(\mathbf{H}, \mathbf{S}_{i,j}^k) - \delta > 0 \quad f: e_{i,j}^k \rightarrow e_{i,j}, x_{i,j} = 1 \quad (7)$$

210



211

212

Fig.4 Safety gap of ROF distance calculations

213

214 3. Development of Optimization Objective Functions

215 The aim of ROF route planning is to select a safe route while reducing the transport costs. The
 216 following sections describe transport costs and extra costs that should be taken into consideration to
 217 find a safe and economic ROF route in the decision-making process.

218

219 3.1 Calculation of transport costs

220 The transport costs are usually calculated based on the distance from original station to destination
 221 station. Let $d_{i,j}$ and $d_{i,j}^k$ denote the distances of the railway section $e_{i,j}$ between two key stations v_i
 222 and v_j and its intersection $e_{i,j}^k$, which can be calculated by

223

$$d_{i,j} = \sum_{f: e_{i,j}^k \rightarrow e_{i,j}} d_{i,j}^k, e_{i,j}^k \in \mathbf{E}', e_{i,j} \in \mathbf{E} \quad (8)$$

225

226 The total distance of a ROF transport route is $\sum_{\forall e_{i,j} \in \mathbf{E}} (x_{i,j} d_{i,j})$ (km) and the transport costs can be
 227 calculated by

228

$$229 \quad Dis_{i,j} = \sum_{\forall e_{i,j} \in E} (x_{i,j} d_{i,j}) \quad (9)$$

$$230 \quad Cost_{i,j} = \omega \mu \sum_{\forall e_{i,j} \in E} (x_{i,j} d_{i,j}) \quad (10)$$

231

232 where ω and μ denote the weight (tons) and the price (USA\$/t-km), respectively.

233 However, the price may include floating cost charges due to oversized loading of a ROF train
234 according to floating cost rate ε based on classification of the out-of-gauge grades. Currently, out-of-
235 gauges are classified in to three grades, i.e., the first out-of-gauge grade, second out-of-gauge grade
236 and super out-of-gauge grade [15]. As can be seen in Fig. 5, the ROF loading outline is represented by
237 the solid line. If the distance between ROF loading outline and railway gauge (the double dot dash line)
238 is more than 1250 mm, but not beyond the first standard gauge (the dot line), the ROF is classified as
239 the first out-of-gauge grade. However, if the distance between ROF loading outline and railway gauge
240 exceeds the first standard gauge (the dot line) and the distance between ROF loading outline and
241 railway gauge in the range of 150 to 1250 mm, but not beyond the second standard gauge (the dot dash
242 line), the ROF is classified as the second out-of-gauge grade. If the distance between ROF loading
243 outline and railway gauge is beyond the second standard gauge (the dot dash line), the ROF is classified
244 as super out-of-gauge grade. The higher the grade of out-of-gauge is, the higher the extra charge would
245 be.

246 Therefore, the basic cost f_{basic} based on the price and floating cost rate can be calculated by

247

$$248 \quad f_{basic} = \omega \mu (1 + \varepsilon) \sum_{\forall e_{i,j} \in E} (x_{i,j} d_{i,j}) \quad (11)$$

249

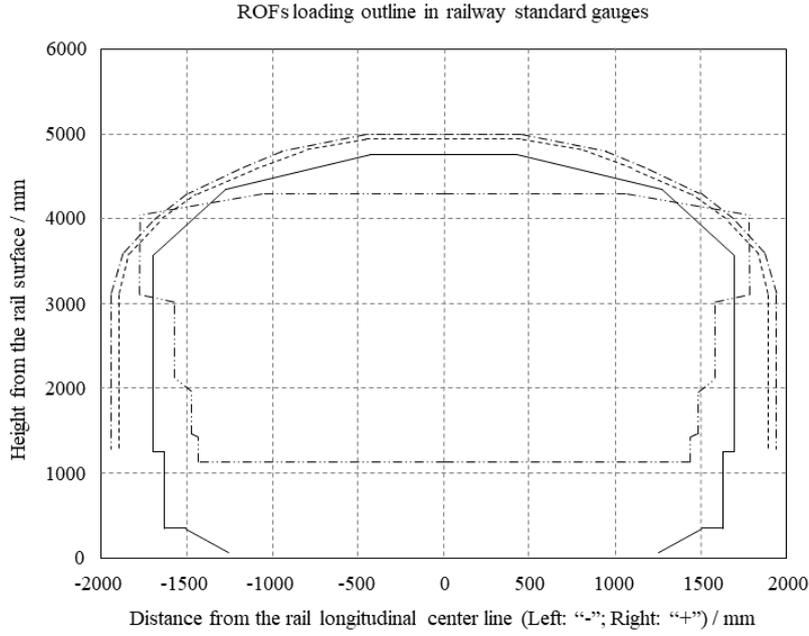


Fig.5 Railway standard gauges Vs ROF out-of-gauge grades

250

251

252

253 3.2 Calculation of extra costs

254 Different safety gaps between ROF loading outlines and railway gauges may have special safe
 255 operation requirements for a ROF train, for example, to limit ROF train's speed and reduce numbers
 256 of other trains running along the ROF route [4, 7]. Therefore, a ROF safe transport may require extra
 257 costs because of speed limit, non-intersection transport, ROF transport with insulating plates and no-
 258 electricity in over-head equipment.

259 Let τ_{sp} , τ_{ni} , τ_{ip} and τ_{nep} be ROF extra cost rates for per intersection along the ROF route
 260 because of speed limit, non-intersection transport, ROF transport with insulating plates and no-
 261 electricity in over-head equipment, respectively, and n_{sp} , n_{ni} , n_{ip} and n_{nep} denote the numbers
 262 of corresponding intersections with the operation requirements. The extra cost f_{extra} can be
 263 calculated by

264

$$265 \quad f_{extra} = \tau_{sp}n_{sp} + \tau_{ni}n_{ni} + \tau_{ip}n_{ip} + \tau_{nep}n_{nep} \quad (12)$$

266

267 where n_{sp} , n_{ni} , n_{ip} and n_{nep} can be determined as below.

268

269 The numbers of intersections with ROF speed limit n_{sp} can be calculated by

270

$$n_{sp} = \sum_{\forall e_{i,j} \in E} (x_{i,j} |\{e_{i,j}^k | dis(\mathbf{H}, \mathbf{S}_{i,j}^k) - \delta \in [d_{sp}^l, d_{sp}^u]\}|) \quad (13)$$

272

273 where $[d_{sp}^l, d_{sp}^u]$ ($d_{sp}^u > d_{sp}^l > 0$) indicates the distance in a railway section for speed limit of a ROF
 274 train, and \mathbf{H} is ROF loading outlines and $\mathbf{S}_{i,j}^k$ is the minimum railway gauges as described before in
 275 section 2.2.

276

277 Let h_{ni} be the gap between The ROF train and other train passing each other, n_{ni} can be
 278 calculated by

279

$$n_{ni} = \sum_{\forall e_{i,j} \in E} (x_{i,j} |\{e_{i,j}^k | h_{ni} - \mathbf{H} - \delta < d_{ni}\}, v_a \in [v_{ni}^l, v_{ni}^u]\}) \quad (14)$$

281

282 Where d_{ni} is the minimum gap clearance for two adjacent trains in the section, and $[v_{ni}^l, v_{ni}^u]$ ($v_{ni}^u >$
 283 $v_{ni}^l > 0$) indicates the range of required speed for non-intersection transport, and v_a is the speed limit
 284 of the other train running on the adjacent line to ROF line.

285

286 Let h_{ecl} be the lowest height of the over-head equipment. Thus, n_{ip} and n_{nep} can be
 287 calculated by Eqs. (15) and (16), respectively.

288

$$n_{ip} = \sum_{\forall e_{i,j} \in E} (x_{i,j} |\{e_{i,j}^k | h_{ecl} - h_{0,0} - \delta \in [d_{ip}^l, d_{ip}^u], \rho_{i,j}^k = 1\}|) \quad (15)$$

290

291 where $[d_{ip}^l, d_{ip}^u]$ ($d_{ip}^u > d_{ip}^l > 0$) indicates distance of the section that a safe gap is required between
 292 ROF outline and insulating plates (plates on the top of the ROF to separate ROF goods from the over-
 293 head equipment), and $\rho_{i,j}^k$ denotes whether or not such an intersection is railway electrification
 294 intersection. When $e_{i,j}^k$ is a railway electrification intersection, $\rho_{i,j}^k = 1$, otherwise, $\rho_{i,j}^k = 0$.

295

$$n_{nep} = \sum_{\forall e_{i,j} \in E} (x_{i,j} |\{e_{i,j}^k | h_{ecl} - h_{0,0} - \delta \in [d_{nep}^l, d_{nep}^u], \rho_{i,j}^k = 1\}|) \quad (16)$$

297

298 where $[d_{nep}^l, d_{nep}^u]$ indicate the distance that a safe gap is required between ROF outline and over-
 299 head equipment with insulating plates, and $d_{ip}^u > d_{ip}^l > d_{nep}^u > d_{nep}^l > 0$.

300 Therefore, the total cost $f(v_o, v_d)$ of a ROF transport from original station to destination station
 301 can be calculated by

$$302 \quad f(v_o, v_d) = f_{\text{basic}} + f_{\text{extra}} \quad (17)$$

303
 304
 305 where v_o is the original station and v_d is the destination station.

306

307 **4. ROF Route Optimal Model**

308 An optimal model can be established to minimize total transport cost with the constraints of ROF
 309 flow balance and railway safety gap clearances as

310

$$311 \quad \text{Min: } f(v_o, v_d) = \omega\mu(1 + \varepsilon) \sum_{\forall e_{i,j} \in E} (x_{i,j} d_{i,j}) + \tau_{\text{sp}} n_{\text{sp}} + \tau_{\text{ni}} n_{\text{ni}} + \tau_{\text{ip}} n_{\text{ip}} + \tau_{\text{nep}} n_{\text{nep}}$$

$$312 \quad \text{Subject to: } \sum_{v_j \in \varphi(v_i)} x_{i,j} - \sum_{v_j \in \beta(v_i)} x_{i,j} = \begin{cases} 1 & v_i = v_o \\ 0 & v_i \neq v_o, v_d \\ -1 & v_i = v_d \end{cases}$$

$$313 \quad \text{dis}(\mathbf{H}, \mathbf{S}_{i,j}^k) - \delta > 0 \quad f: e_{i,j}^k \rightarrow e_{i,j}, x_{i,j} = 1$$

$$314 \quad x_{i,j} = 1 \text{ or } 0 \quad (18)$$

315

316 Therefore, the optimal ROF transport route \mathbf{R}^* ($\mathbf{R}^* \subseteq E$) in the ROF key network \mathbf{G} can be calculated
 317 by

318

$$319 \quad \mathbf{R}^* = \{e_{i,j} | e_{i,j} \in E, x_{i,j} = 1\} \quad (19)$$

320

321 and the optimal intersection set \mathbf{R}'^* ($\mathbf{R}'^* \subseteq E'$) in the whole freight network \mathbf{G}' can be determined by

322

$$323 \quad \mathbf{R}'^* = \{e_{i,j}^k | e_{i,j}^k \in E', e_{i,j} \in \mathbf{R}^*, f: e_{i,j}^k \rightarrow e_{i,j}\} \quad (20)$$

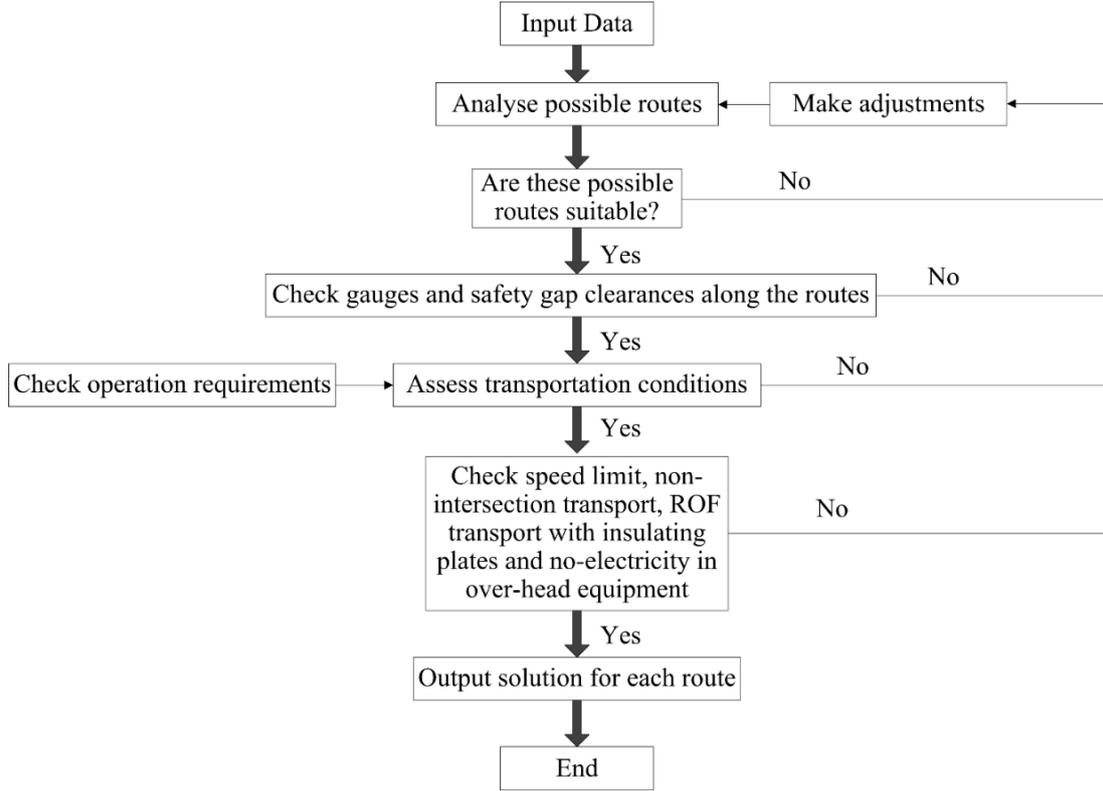
324

325 **5. Proposed ROF Safe and Economic Transportation Route Decision Support Process**

326 As described earlier in this paper, it is necessary to develop a ROF transportation decision support
 327 process for selection of a safe and economic route for a ROF train [7, 15]. Fig. 6 shows the proposed

328 ROF safe and economic route decision support process that is described in the follow sections.

329



330

331

Fig.6 Proposed ROF safe and economic transportation route decision support process

332

333

5.1 Possible ROF transport route generation

334

The process of possible ROF transport route generation is summarized in Table 2, which can be done based on historical database [19-21]. However, as stated earlier in this paper, the data of railway gauges are always changed in real time across railway network according to current actual situations. therefore, Double-checking approach by taking current field investigation data into consideration needs to be applied to ensure the possible ROF transport routes are safe, which is discussed in Section 5.2 [22].

339

Table 2 Possible ROF transport route generation

Inputs: ROF key network \mathbf{G} , the freight network \mathbf{G}' , distance of the key section $d_{i,j}$ (km), ROF original station v_o and destination station v_d ; maximum ROF outline middle-center height h_{max} , maximum half-width w_{max} , historical ROF transport data \mathbf{R}_{data} , and setting up judgment criteria of height Δd_h (mm) and width Δd_w (mm).

Outputs: Possible transport route set of \mathbf{R}_{pos} in ROF key network \mathbf{G} , and possible intersection set of \mathbf{R}'_{pos} in the whole freight network \mathbf{G}' .

Step 1: Assume $\mathbf{R}_{old} = \emptyset$, check possible transport routes from historical database whether or not similar routes are in historical route set of \mathbf{R}_{data} including original stations, destination stations, maximum middle-center heights and maximum half-widths of ROF outlines denoted by v_{odata} , v_{ddata} , h_{data} and w_{data} (mm). There are three conditions C1, C2 and C3:

C1: Check whether or not the original and destination stations are the same or they locate at the same key sections:

$$v_o(f: e_{i,j}^k \rightarrow e_{i,j}) = v_{odata}(f: e_{i,j}^k \rightarrow e_{i,j}), v_d(f: e_{i,j}^k \rightarrow e_{i,j}) = v_{ddata}(f: e_{i,j}^k \rightarrow e_{i,j})$$

and

$$v_o(f: e_{i,j}^k \rightarrow e_{i,j}) = v_{odata}(f: e_{i,j}^k \rightarrow e_{i,j}), \quad v_d(f: e_{i,j}^k \rightarrow e_{i,j}) = v_{odata}(f: e_{i,j}^k \rightarrow e_{i,j})$$

C2: Check the maximum middle-center height deviation of the historical ROF outlines data and compare with the current ROF outline is less than Δd_h (mm), i.e.,

$$|h_{max} - h_{data}| \leq \Delta d_h$$

C3: Check the maximum half-width deviation of the historical ROF outlines and compare with the current ROF outline is less than Δd_w (mm) or not, i.e.,

$$|w_{max} - w_{data}| \leq \Delta d_w$$

If above three conditions of C1, C2, and C3 satisfy the requirements, the historical route set \mathbf{R}_{data} will be possible transport routes for the current ROF train, i.e., $\mathbf{R}_{old} = \mathbf{R}_{old} \cup \{\mathbf{R}_{data}\}$.

Step 2: Calculate the k^{th} possible route \mathbf{R}_{new} of current ROF train. Let \mathbf{R}_{old} denote historical routes and \mathbf{R}_{new} are current possible routes, if the set \mathbf{R}_{old} does not satisfy the requirements, then to generate new possible ROF transport routes set \mathbf{R}_{new} by using the k' -shortest algorithm ($k' < k$) [21].

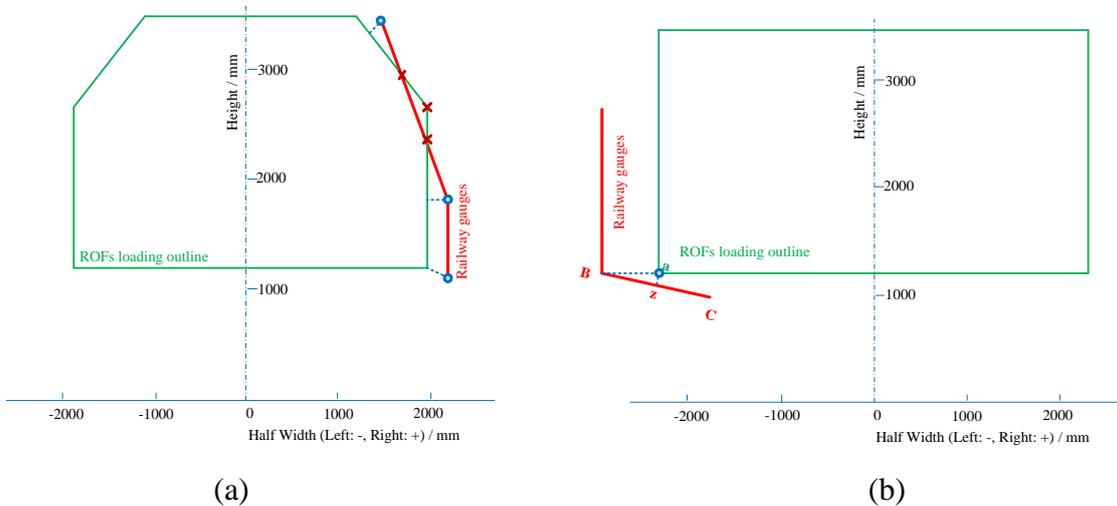
Step 3: Determine $\mathbf{R}_{pos} = \mathbf{R}_{old} \cup \mathbf{R}_{new}$.

Step 4: Calculate $f: e_{i,j}^k \rightarrow e_{i,j}$ between the networks \mathbf{G} and \mathbf{G}' to ensure each intersection in the possible intersection set of \mathbf{R}'_{pos} within the ROF network \mathbf{G}' .

340

341 5.2 Double-checking approach to check railway gauges, safety gap clearances and operation 342 conditions along the possible routes

343 It is important to ensure that safety gaps between ROF loading outlines and railway gauges in the
344 planned ROF route satisfy safety requirements. If the gap distances between ROF loading outlines and
345 railway gauges are calculated only based on control points as described in Section 2.2, it could be
346 potential risks leading to accidents. For example, Fig. 7 (a) shows a potential risk (the red cross points)
347 where a gap distance between a ROF loading outline and railway gauges is calculated based on control
348 points of railway gauges, which is not correct, and Fig.7 (b) shows a case that the shortest gap distance
349 is $|az|$, but not $|aB|$, i.e., $|az| < |aB|$.



350

351

352

Fig.7 Calculations of different gap distances

353

354 Therefore, the gap distances should be calculated by using both actual control points of ROF
355 loading outlines and railway gauges, in other words, double-checking approach should be applied.
356 Table 3 shows the process of the proposed double-checking approach to calculate correct gap distances.
357 In double-check approach, a minimum gap d_{fix} and safety allowance δ need to be defined to control
358 the gap distances, for example, $d_{\text{fix}} = 300\text{mm}$ and $\delta = 10\text{mm}$ are currently used to define the
359 minimum gap and safety allowance. As described in Section 2.2, initial gap distances d_{temp} based on
360 control points of ROF loading outlines \mathbf{H} and railway gauges \mathbf{S}_{ij}^k can be calculated. If $d_{\text{temp}} < d_{\text{fix}}$,
361 the loading outlines need to be re-planned. If $d_{\text{temp}} \geq d_{\text{fix}}$, then the gap distance sets will be $\mathbf{g}_H =$
362 $\mathbf{g}_H \cup \{d_{\text{temp}} - \delta\}$ determined by ROF loading outlines and $\mathbf{g}_S = \mathbf{g}_S \cup \{d_{\text{temp}} - \delta\}$ determined by
363 control points of railway gauges, and then save the \mathbf{g}_H and \mathbf{g}_S to control point set \mathbf{g}_{cpl} . Finally,
364 minimum safety gap distance can be calculated as $d_{\text{gap}} = \min\{\mathbf{g}_H \cup \mathbf{g}_S\}$, and control points can be
365 determined as $L_{\text{gap}} = \{l_{\text{gap}} | l_{\text{gap}} \in \mathbf{g}_{\text{cpl}}, d_{\text{temp}} = d_{\text{gap}}\}$.

366

367 **Table 3 Double-checking Approach**

Inputs: ROF loading outlines \mathbf{H} , railway gauges \mathbf{S}_{ij}^k , defined safety gap d_{fix} and safety allowance δ .

Outputs: Safety gap distance d_{gap} (mm), and control point L_{gap} .

Step 1: Assume initial safety gap distance set d_{temp} that are calculated based on control points of ROF loading outlines to be \mathbf{g}_H , and safety gap distance set that are calculated based on control points of railway gauges to be \mathbf{g}_S , and control points set \mathbf{g}_{cpl} , $d_{\text{temp}} = 0$ and $d_{\text{gap}} = 0$.

Step 2: Calculate initial gap distance d_{temp} based on control points of ROF loading outlines \mathbf{H} and railway gauges \mathbf{S}_{ij}^k as described in Section 2.2. If $d_{\text{temp}} < d_{\text{fix}}$, the loading outlines need to be re-planned; If $d_{\text{temp}} \leq d_{\text{fix}}$, then $\mathbf{g}_H = \mathbf{g}_H \cup \{d_{\text{temp}} - \delta\}$ and $\mathbf{g}_S = \mathbf{g}_S \cup \{d_{\text{temp}} - \delta\}$, and save the \mathbf{g}_H and \mathbf{g}_S into the control point set \mathbf{g}_{cpl} .

Step 3: Calculate minimum safety gap distance $d_{\text{gap}} = \min\{\mathbf{g}_H \cup \mathbf{g}_S\}$.

Step 4: Determine control points $L_{\text{gap}} = \{l_{\text{gap}} | l_{\text{gap}} \in \mathbf{g}_{\text{cpl}}, d_{\text{temp}} = d_{\text{gap}}\}$.

368

369 The results produced from double-checking approach for railway gauges and safety gap clearances
370 along the routes based on both of ROF loading outlines and railway gauges provide useful information
371 for selection of safe ROF routes.

372

373 **5.3 Optimization of ROF routes**

374 A safe ROF route may not be an economic one. Therefore, all of possible safe routes produced as
 375 described in Sections 5.1 and 5.2 need to be further examined by taking transportation costs into
 376 consideration to select a safe and economic ROF route by using Eqs. (18), (19) and (20) as stated in
 377 Section 4.

378

379 The process of the developed optimization of ROF routes is summarized in Table 4.

380 **Table 4** Optimization of ROF routes

Inputs: ROF key network $\mathbf{G} = (\mathbf{V}, \mathbf{E})$, the freight network $\mathbf{G}' = (\mathbf{V}', \mathbf{E}')$, distance of each intersection $d_{i,j}^k$ (km), railway electrification intersection $\rho_{i,j}^k$, the lowest height of over-head equipment h_{ecl} (mm), minimum gauge of each intersection $S_{i,j}^k$ (mm), safety allowance of the gap clearance δ (mm), ROF original station v_o and destination station v_d , ROF loading outlines \mathbf{H} (mm), ROF weight ω (tons), transport price rate per ton per kilometer μ , price floating rate ε , ROF extra transport cost per intersection τ_{sp} , τ_{ni} , τ_{ip} and τ_{nep} , the distances of safe operation requirements d_{sp}^l , d_{sp}^u , d_{ip}^l , d_{ip}^u , d_{nep}^l , and d_{nep}^u (mm), judgment criteria of height Δd_h (mm) and width Δd_w (mm), historical ROF transport data \mathbf{R}_{data} .

Outputs: The optimal ROF transport route \mathbf{R}^* , optimal intersection set \mathbf{R}'^* , costs of objective functions $Min: f(v_o, v_d)$, and n_{sp} , n_{nm} , n_{ip} , n_{nep} , f_{basic} , f_{extra} and corresponding operation requirements.

Step 1: Initialization

Set up initial $x_{i,j} = 0 (\forall e_{i,j} \in \mathbf{E})$, ROF middle-center height $h_{max} = h_{0,0}$, ROF maximum half-width $w_{max} = \max\{w_0, w_1, \dots, w_n\}$, $n_{sp} = 0$, $n_{ni} = 0$, $n_{ip} = 0$, $n_{nep} = 0$, $f_{basic} = 0$, $f_{extra} = 0$, $f(v_o, v_d) = 0$, $\mathbf{R}^* = \emptyset$, $\mathbf{R}'^* = \emptyset$, and calculate the distance of each key section $d_{i,j}$ (km) by using Eq. (8).

Step 2: Generation of possible ROF transport routes

Generate possible ROF transport route set \mathbf{R}_{pos} in the ROF key network \mathbf{G} and possible intersections set \mathbf{R}'_{pos} in the whole freight network \mathbf{G}' as described in Section 5.1.

Step 3: Checking gauges, safety gap clearances and operation conditions along the possible routes

Step 3.1: Assign initial route $b = 1$, and unsafe routes set $\mathbf{R}_{us} = \emptyset$.

Step 3.2: For the b^{th} route \mathbf{r}_b in \mathbf{R}_{pos} (\mathbf{r}'_b in \mathbf{R}'_{pos}) and $x_{i,j}^b = 0 (\forall e_{i,j} \in \mathbf{E})$; If $e_{i,j} \in \mathbf{r}_b$, $x_{i,j}^b = 1$, then assign $n_{ni}^b = 0$, $n_{ip}^b = 0$, $n_{nep}^b = 0$, $f_{basic}^b = 0$, $f_{extra}^b = 0$, $f^b(v_o, v_d) = 0$, $\mathbf{r}_{sp}^b = \emptyset$, $\mathbf{r}_{ni}^b = \emptyset$, $\mathbf{r}_{ip}^b = \emptyset$ and $\mathbf{r}_{nep}^b = \emptyset$. Otherwise, $x_{i,j}^b = 0$.

Step 3.3: Calculate the minimum gap distance d_{gap}^b , the gap height h_{gap} between ROF middle-center height and the lowest height of over-head equipment, i.e., $h_{gap}^b = h_{ecl} - h_{max} - \delta$ as described in Section 5.2.

Step 3.4: If ROF non-intersection transport occurs in the intersection $e_{i,j}^k$, then $n_{ni}^b = n_{ni}^b + 1$ and $\mathbf{r}_{ni}^b = \mathbf{r}_{ni}^b \cup \{e_{i,j}^k\}$;

If $d_{gap}^b \in [d_{sp}^l, d_{sp}^u]$, then $n_{sp}^b = n_{sp}^b + 1$, $\mathbf{r}_{sp}^b = \mathbf{r}_{sp}^b \cup \{e_{i,j}^k\}$;

If $d_{gap}^b \leq 0$, then $n_{us}^b = n_{us}^b + 1$, $\mathbf{r}_{us}^b = \mathbf{r}_{us}^b \cup \{e_{i,j}^k\}$, $\mathbf{R}_{us} = \mathbf{R}_{us} \cup \{\mathbf{r}_b\}$;

If $h_{gap}^b \in [d_{ip}^l, d_{ip}^u]$ and $\rho_{i,j}^k = 1$, then $n_{ip}^b = n_{ip}^b + 1$, $\mathbf{r}_{ip}^b = \mathbf{r}_{ip}^b \cup \{e_{i,j}^k\}$;

If $h_{\text{gap}}^b \in [d_{\text{nep}}^l, d_{\text{nep}}^u]$ and $\rho_{i,j}^k = 1$, then $n_{\text{nep}}^b = n_{\text{nep}}^b + 1$, $\mathbf{r}_{\text{nep}}^b = \mathbf{r}_{\text{nep}}^b \cup \{e_{i,j}^k\}$.

Step 3.5: Calculate the total distance $d_{\text{total}}^b = \sum_{x_{i,j}^b=1} |d_{i,j}|$ between original station and destination station, and the objective function f_{basic}^b , f_{extra}^b , $f^b(v_o, v_d)$ by using Eqs. (11), (12) and (17).

Step 3.6: $b = b + 1$, if $b \leq |\mathbf{R}_{\text{pos}}|$, turn to *Step 3.2*; otherwise, turn to *Step 4*.

Step 4: Evaluation and selection

If $\mathbf{r}_{b'} \in \mathbf{R}_{\text{pos}}$ ($\mathbf{r}'_{b'} \in \mathbf{R}'_{\text{pos}}$), $\forall \mathbf{r}_b \in \mathbf{R}_{\text{pos}}$ ($\mathbf{r}_b \neq \mathbf{r}_{b'}, \mathbf{r}'_b \in \mathbf{R}'_{\text{pos}}$), and $f^{b'}(v_o, v_d) \leq f^b(v_o, v_d)$, then output $n_{\text{sp}} = n_{\text{sp}}^{b'}$, $n_{\text{ni}} = n_{\text{ni}}^{b'}$, $n_{\text{ip}} = n_{\text{ip}}^{b'}$, $n_{\text{nep}} = n_{\text{nep}}^{b'}$, $f_{\text{basic}} = f_{\text{basic}}^{b'}$, $f_{\text{extra}} = f_{\text{extra}}^{b'}$, $\text{Min } f(v_o, v_d) = f^{b'}(v_o, v_d)$, $\mathbf{R}^* = \mathbf{r}_{b'}$, $\mathbf{R}'^* = \mathbf{r}'_{b'}$, and ROF operation requirements in intersections $\mathbf{r}_{\text{sp}}^{b'}$, $\mathbf{r}_{\text{ni}}^{b'}$, $\mathbf{r}_{\text{ip}}^{b'}$ and $\mathbf{r}_{\text{nep}}^{b'}$.

381

382 As can be seen in Table 4, double-checking approach and determination of gap distance as
 383 described in Sections 5.1 and 5.2 are applied to reflect safe operation requirements together with
 384 transport cost consideration as described in Section 3 to minimize the total cost of the ROF
 385 transportation so that a safe and economic ROF transport route can be determined. A case study is used
 386 to demonstrate the application of the proposed railway ROF transport routing optimal methodology.

387

388 6. Case Study

389 This section presents a case study to demonstrate the application of the proposed methodology.

390 6.1 Background

391 A ROF train is loaded with the highest/lowest car floor's height 1250/1170 (mm) with car bogie
 392 center distance 9000 (mm), the details of such a ROF train are shown in Table 5 and loading outlines
 393 are shown in Table 6.

394

395 **Table 5** Details of ROF train

Items	Data
Original station	v_o (a key station)
Destination station	v_d (an intermediate station)
Weight (tons)	52.0
Length (mm)	12500
Maximum width (mm)	1830 (both sides)
Maximum height (mm)	4250
Out-of-gauge grade	Super

396

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Table 6 ROF loading outlines

Location	Higher height (mm)	Lower height (mm)	Half-width (mm)
Middle-center height	4250	-	1231
1 st -side height	4050	3290	1780
2 nd -side height	3050	2170	1830
3 rd -side height	1970	1470	1480
4 th -side height	1470	1170	1400

400 The ROF train is planned to run from original station v_o to destination station v_d . Fig. 8 shows
 401 all intermediate stations in the whole freight network G' , and connections of all key stations represented
 402 by blue circles that form the ROF key network G . The distances between key stations and intermediate
 403 ones are shown in Table 7.

404 According to historical ROF transport data and current existing railway gauges, $\delta = 40$ mm,
 405 $\Delta d_h = 40$ mm, $\Delta d_w = 20$ mm; $d_{sp}^l = 70$ mm, $d_{sp}^u = 150$ mm, $d_{ip}^l = 100$ mm, $d_{ip}^u = 350$ mm,
 406 $d_{nep}^l = 50$ mm, $d_{nep}^u = 100$ mm, and $h_{ecl} = 5700$ mm, and the price rate $\mu = 0.02239$ USA\$/per
 407 ton per kilometer can be obtained.

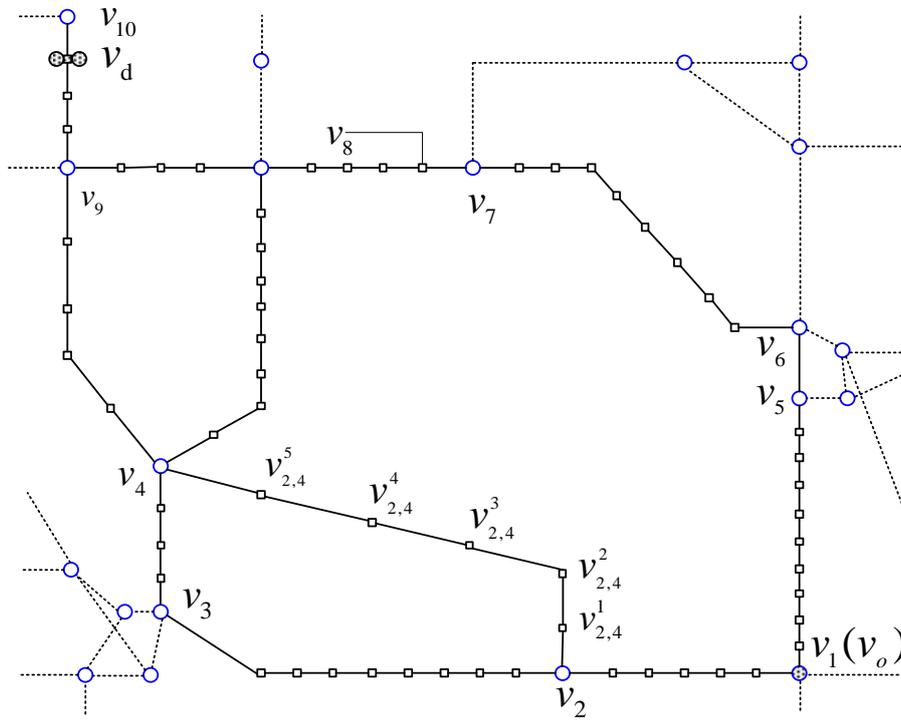


Fig.8 ROF freight network G'

Table 7 Distances and relationships between different stations in networks G' and G

Intersections	Key sections (railway stations)	Relationship between two railway stations	Intersections number	Distance (km)	
				Intersections	Between two key section
$e_{1,2}$	$v_1(v_0) \rightarrow v_2$	$v_{1,2}^1, v_{1,2}^2, v_{1,2}^3, v_{1,2}^4, v_{1,2}^5$	6	11, 17, 11, 25, 12, 17	93
$e_{1,5}$	$v_1 \rightarrow v_5$	$v_{1,5}^1, v_{1,5}^2, v_{1,5}^3, v_{1,5}^4, v_{1,5}^5,$ $v_{1,5}^6, v_{1,5}^7, v_{1,5}^8, v_{1,5}^9$	10	30, 29, 31, 23, 23, 50, 27, 27, 30, 13	115
$e_{2,3}$	$v_2 \rightarrow v_3$	$v_{2,3}^1, v_{2,3}^2, v_{2,3}^3, v_{2,3}^4, v_{2,3}^5,$ $v_{2,3}^6, v_{2,3}^7, v_{2,3}^8$	9	8, 18, 12, 15, 12, 9, 16, 12, 4	106
$e_{2,4}$	$v_2 \rightarrow v_4$	$v_{2,4}^1, v_{2,4}^2, v_{2,4}^3, v_{2,4}^4, v_{2,4}^5$	6	5, 7, 11, 35, 19, 34	111
$e_{3,4}$	$v_3 \rightarrow v_4$	$v_{3,4}^1, v_{3,4}^2, v_{3,4}^3$	4	32, 23, 33, 25	113
$e_{4,8}$	$v_4 \rightarrow v_8$	$v_{4,8}^1, v_{4,8}^2, v_{4,8}^3, v_{4,8}^4, v_{4,8}^5,$ $v_{4,8}^6, v_{4,8}^7, v_{4,8}^8$	9	7, 23, 11, 23, 21, 12, 23, 22, 13	155
$e_{4,9}$	$v_4 \rightarrow v_9$	$v_{4,9}^1, v_{4,9}^2, v_{4,9}^3, v_{4,9}^4$	5	49, 51, 15+2, 27, 6	150
$e_{5,6}$	$v_5 \rightarrow v_6$	-	1	9	9
$e_{6,7}$	$v_6 \rightarrow v_7$	$v_{6,7}^1, v_{6,7}^2, v_{6,7}^3, v_{6,7}^4, v_{6,7}^5,$ $v_{6,7}^6, v_{6,7}^7, v_{6,7}^8$	9	12, 15, 14, 16, 14, 13, 23, 20, 18	145
$e_{7,8}$	$v_7 \rightarrow v_8$	$v_{7,8}^1, v_{7,8}^2, v_{7,8}^3, v_{7,8}^4$	5	7, 8, 22, 26, 9	72
$e_{8,9}$	$v_8 \rightarrow v_9$	$v_{8,9}^1, v_{8,9}^2, v_{8,9}^3$	4	24, 14, 49, 31	118
$e_{9,10}$	$v_9 \rightarrow v_{10}$	$v_{9,10}^1, v_{9,10}^2, v_{9,10}^3$	4	38, 39, 13, 6	96
$e_{9,d}$	$v_9 \rightarrow v_d$	$v_{9,d}^1, v_{9,d}^2$	3	38, 39, 13	90
$e_{d,10}$	$v_d \rightarrow v_{10}$	-	1	6	6

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416 6.2 Selection of the safe and economic ROF route

417 As such a ROF train is classified as a super out-of-gauge grade, the price floating rate is $\varepsilon = 10\%$. In

418 this case, assign $n_{ni} = 0$, then $\tau_{nm}n_{ni} = 0$, i.e., other trains can run in the sections along the route.

419 There is not a railway electrification intersection $e_{i,j}^k$ in the possible routes, i.e., $\rho_{i,j}^k = 0$, in other

420 words, no over-head equipment along the possible routes. The gap distance h_{gap} between ROF

421 middle-center height $h_{0,0}$ and the lowest height of h_{ecl} can be calculated $h_{\text{gap}} = h_{\text{ecl}} - h_{0,0} - \delta =$

422 $5700 - 4250 - 40 = 1410$ mm, therefore, $h_{\text{gap}} \notin [d_{\text{ip}}^l, d_{\text{ip}}^u] = [100\text{mm}, 350\text{mm}]$,

423 $h_{\text{gap}} \notin [d_{\text{nep}}^l, d_{\text{nep}}^u] = [50\text{mm}, 100\text{mm}]$, $n_{\text{ip}} = 0$ and $n_{\text{nep}} = 0$. The extra transport costs caused by

424 using Eq. (15) and (16) are 0, i.e., $h_{\text{gap}} \geq 350\text{mm}$, $\tau_{\text{ip}}n_{\text{ip}} = 0$, and $\tau_{\text{nep}}n_{\text{nep}} = 0$.

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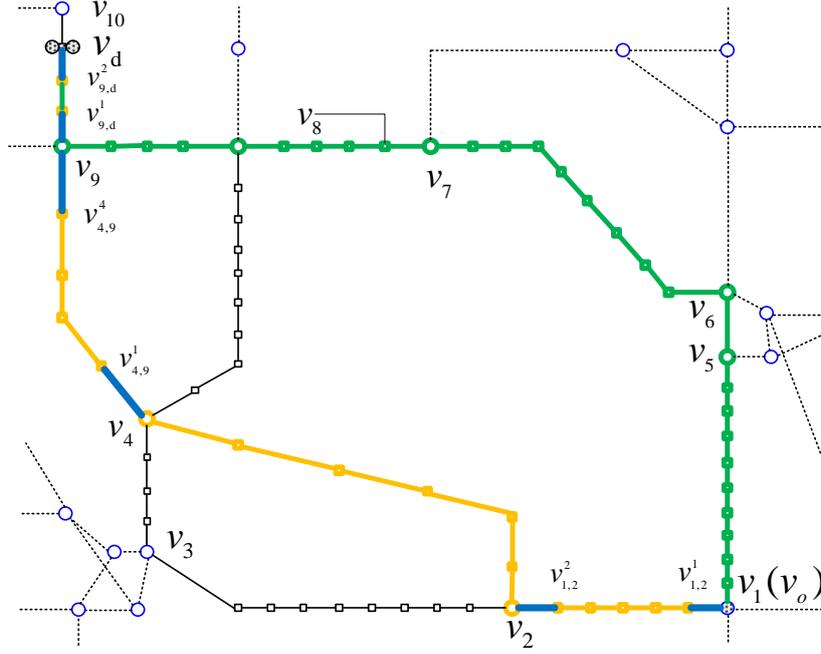


Fig.9 Possible ROF transport routes and operation requirements

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There are two possible routes generated as described in Section 5.1, i.e., the Route 1: $v_o(v_o = v_1) \rightarrow v_2 \rightarrow v_4 \rightarrow v_9 \rightarrow v_d$ with 444km and 20 intersections, and the Route 2: $v_o(v_o = v_1) \rightarrow v_5 \rightarrow v_6 \rightarrow v_7 \rightarrow v_8 \rightarrow v_9 \rightarrow v_d$ with 717 km and 30 intersections as shown in Fig. 9. There are six intersections in the Route 1 and two intersections in the Route 2 where the ROF train should control its speed as shown in Fig. 9 as blue lines. Therefore, extra charges will be applied for these sections because of speed limit. Fig. 10 shows an example of the calculation of gap distances between ROF loading outlines and the minimum railway gauges at the intersection $(v_{9,d}^1, v_{9,d}^2)$. The minimum gap distance is 118.71 mm and $d_{\text{gap}} = 118.71 - \delta = 118.71 - 40 = 78.71 \in [d_{\text{sp}}^l, d_{\text{sp}}^u] = [70\text{mm}, 150\text{mm}]$. Therefore, speed control is required based on operation conditions in the intersection $(v_{9,d}^1, v_{9,d}^2)$ for both of Routes 1 and 2. According to Eq. (17), the total cost of Routes 1 and 2 can be calculated by $f^1(v_o, v_d) = 568.73 + 6\tau_{\text{sp}}$ and $f^2(v_o, v_d) = 918.41 + 2\tau_{\text{sp}}$, respectively, which speed limit is assigned as 15km/h and extra cost rate at USA\$87.422/km, in this case, $f^1(v_o, v_d) > f^2(v_o, v_d)$.

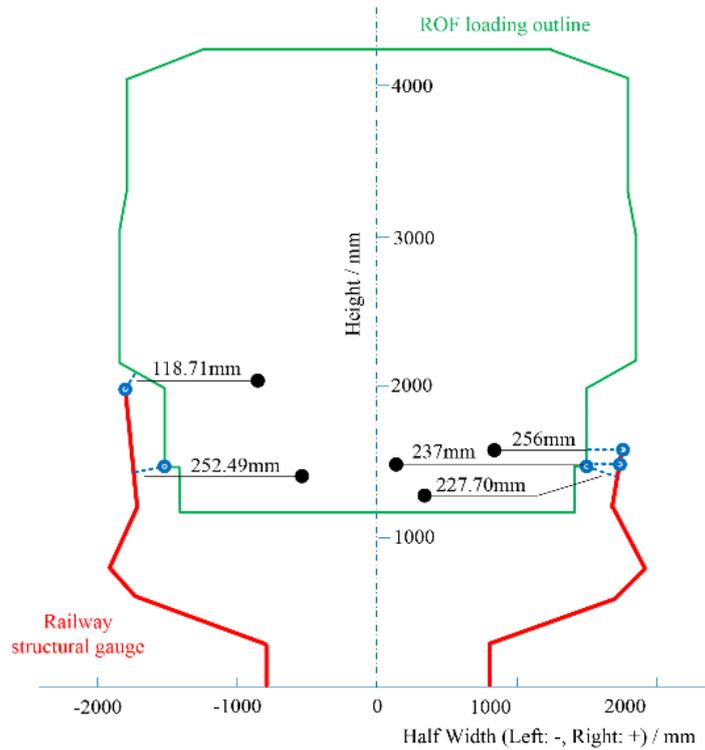


Fig.10 Gap distance calculation at the intersection ($v_{9,d}^1, v_{9,d}^2$)

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Table 8 summarizes results of Routes 1 and 2. As can be seen that the selection of the best safe and economic route is determined mainly based on the safety gap distance between ROF loading outlines and railway gauges along its route, the total distance of each possible route, weight of the ROF train, basic transport cost, and the extra transport cost. In this case, Route 2 is the best ROF safe and economic transport route.

Table 8 Comparison results between Routes 1 and 2

Calculation results		Route 1	Route 2
ROF transport route (Key station set)		$v_o(v_o = v_1) v_2 v_4 v_9 v_d$	$v_o(v_o = v_1) v_5 v_6 v_7 v_8 v_9 v_d$
Minimum gap clearance (mm)		118.71	118.71
Other 4 lager gap/clearance between ROF loading and railway structural gauges (mm)		227.70	227.70
		237.00	237.00
		252.49	252.49
		256.00	256.00
Speed limit (km/h)		15	15
Normal intersections (Number/Distance(km))		14/310	28/666
Speed limit Intersection (n_{sp} /Distance(km))		6/134	2/51
Routing distance (km)		444	717
Costs of objective function	Basic cost	568.73	918.41
	Extra cost	$6\tau_{sp}$	$2\tau_{sp}$
	$n_{sp}\tau_{sp}$	$6\tau_{sp}$	$2\tau_{sp}$
	$n_{ni}\tau_{ni}$	0.00	0.00

$n_{ip}\tau_{ip}$	0.00	0.00
$n_{nep}\tau_{nep}$	0.00	0.00
Total cost (USA\$)	$f(v_o, v_d) = f_{basic} + f_{extra}$ $= 568.73 + 6\tau_{sp}$	$f(v_o, v_d) = f_{basic} + f_{extra}$ $= 918.41 + 2\tau_{sp}$

453

454 With regards to control ROF train's speed at a number of certain railway intersections, it should
455 be noted that different country has its own regulations. For example, according to *Railway Out-of-*
456 *gauge and Overweight Freight transport Regulations 2016* [9] issued by China National Railway
457 Corporation, if the gap distance is between 100mm and 150mm, a ROF train speed is limited as no
458 more than 25 km/h; if the gap distance is between 70mm and 100mm, a ROF train speed is limited as
459 no more than 15 km/h; if the gap distance is less than 70mm, a ROF train speed is limited as below 5
460 km/h. In this case, the ROF train is limited as 15 km/h because the minimum gap distance is 78.71mm,
461 i.e., $d_{gap} = 118.71 - \delta = 118.71 - 40 = 78.71 \in [d_{sp}^l, d_{sp}^u] = [70mm, 150mm]$.

462 As can also be seen in this case, the shortest route is Route 1 ($v_o \rightarrow v_2 \rightarrow v_4 \rightarrow v_9 \rightarrow v_d$ ($v_o =$
463 v_1)), but the optimal transport route is Route 2 ($v_o \rightarrow v_5 \rightarrow v_6 \rightarrow v_7 \rightarrow v_8 \rightarrow v_9 \rightarrow v_d$ ($v_o = v_1$)) that
464 is a longer route than Route 1. The main reason is related to safety clearances because it causes extra
465 costs due to speed limit, i.e., $f^1(v_o, v_d) > f^2(v_o, v_d)$. The results produced from the proposed method
466 can provide useful information for railway operators to decide in selection of a safe and economic
467 route for the RPF train.

468

469 7. Conclusions

470 Railway out-of-gauge freight is beyond railway gauges in its dimensions, which could be risks leading
471 to serious railway accidents. The selection of a safe and economic route for a ROF train is always a
472 challenge task for railway managers and operators in the planning of ROF routes. This is particular
473 true because ROF route selection decisions have to be made based on safety gap clearances, costs and
474 safe operation requirements. This paper presents a new method for selection of a safe and economic
475 ROF route in which safety and economics are taken into consideration. The proposed method and ROF
476 safe and economic transportation route decision support approach described in this paper can be used
477 to plan ROF routes in which possible routes can be calculated and ranked, and the best safe and
478 economic route can be determined. A case study is presented in this paper to demonstrate the
479 application of the proposed methodology. The results show that the proposed method can provide very

480 useful information for railway operators and managers to choose the best ROF route to meet their
481 objective priorities of safety and economics.

482

483 **Conflicts of Interest**

484 The authors declare that they have no conflicts of interest.

485

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