

Patients with medial knee osteoarthritis reduce medial knee contact forces by altering trunk kinematics, progression speed, and stepping strategy during stair negotiation: A Pilot Study

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23 Abstract

Medial knee loading during stair negotiation in individuals with medial knee osteoarthritis, has 24 only been reported in terms of joint moments, which may underestimate the knee loading. This 25 study assessed knee contact forces (KCF) and contact pressures during different stair 26 negotiation strategies. Motion analysis was performed in five individuals with medial knee 27 osteoarthritis (52.8 ± 11.0 years) and eight healthy subjects (51.0 ± 13.4 years) while ascending 28 29 and descending a staircase. KCF and contact pressures were calculated using a multi-body knee model while performing step-over-step at controlled and self-selected speed, and step-by-step 30 31 strategies. At controlled speed, individuals with osteoarthritis showed decreased peak KCF during stair ascent but not during stair descent. Osteoarthritis patients showed higher trunk 32 rotations in frontal and sagittal planes than controls. At lower self-selected speed, patients also 33 presented reduced medial KCF during stair descent. While performing step-by-step, medial 34 contact pressures decreased in osteoarthritis patients during stair descent. Osteoarthritis 35 patients reduced their speed and increased trunk flexion and lean angles to reduce KCF during 36 stair ascent. These trunk changes were less safe during stair descent where a reduced speed was 37 more effective. Individuals should be recommended to use step-over-step during stair ascent 38 and step-by-step during stair descent to reduce medial KCF. 39

40 *Keywords:* Knee osteoarthritis, motion analysis, knee contact forces, contact pressures,

41 musculoskeletal modeling.

42 Word Count: 3996 words.

43 Introduction

Stair negotiation and level walking are common activities of daily living. However, stair 44 negotiation is biomechanically more challenging ¹, demanding a higher range of motion in the 45 lower extremity², higher moments acting at the knee joint³⁻⁵ and, consequently, increased 46 quadriceps demands compared to level walking. Thus, stair negotiation is particularly 47 demanding for the elderly or subjects with knee osteoarthritis (OA)⁶, who often face the first 48 difficulties in daily task performance and pain complaints ⁷, particularly during stair descent ⁸. 49 However, stair negotiation has not been deeply explored in OA with most studies in literature 50 51 focusing on knee loading during level walking as a biomarker for OA onset and progression. Previous literature has shown reduced knee flexion moments (KFM) ^{4,7,9}, non-conclusive 52 findings in knee adduction moments (KAM)^{4,10} and altered muscle activation patterns ⁶ in 53 severe knee OA patients during stair negotiation. In addition, these patients exhibited higher 54 trunk flexion angles ^{11,12} and hip flexion moments ^{11,13} than healthy subjects while ascending 55 stairs ¹¹. These alterations observed in OA patients have been associated with a loss of 56 quadriceps function ^{14,15} as these muscles provide extensor moments necessary to accelerate 57 the upward propulsive phase occurring during the first part of stair ascent and to decelerate the 58 lowering of the body during stair descent ¹⁶. 59

Generally, healthy and young individuals use a traditional step-over-step motion pattern 60 during stair negotiation, but OA patients frequently feel forced to adjust their stair gait due to 61 62 knee pain, reduced range of motion, muscle weakness, stiffness and instability complaint ^{17,18}. Therefore, they often adopt alternate walking patterns, such as increased handrail use, sideways 63 motion, or a step-by-step patterns (placing both feet on the same step) ^{19,20,21} and/or a 64 significantly reduced speed ^{4,22}. In healthy subjects, the step-by-step strategy has been 65 demonstrated to require higher energy costs and be less efficient than step-over-step, while it 66 seems to increase stability and compensates for lower-limb weakness ^{19,23}. However, 67

significant reductions in KFM were found for the leading leg during step-by-step when compared to step-over-step while descending stairs in healthy subjects, and reduced anteroposterior force for step-by-step versus step-over-step either during stair ascent or descent 23 .

To date it is still unknown how the altered stair negotiation patterns observed in 72 individuals with knee OA affect the compartmental knee contact forces (KCF) as only 73 kinematics and kinetics 4,11,24 have been explored, which do not provide direct measures of 74 cartilage loading. However, KCF reflect not only the influence of external forces but also the 75 76 muscle and ligament forces. Computational approaches are non-invasive, do not alter the knee biomechanics and can be applied to a larger number of subjects compared to in vivo KCF 77 calculations. Therefore, computation of KCF in patients with knee OA during gait has received 78 increasing attention over the last years ²⁵⁻²⁷. Previous research ²⁸ has shown the important role 79 of muscle action controlling flexion-extension and adduction-abduction moments in joint 80 loading, specially, during late stance of gait. This was particularly evident in patients with 81 established knee OA. To our knowledge, however, KCF calculated using musculoskeletal 82 modeling that accounts for muscle and ligament forces in combination with dynamic 83 simulations has never been used in individuals with knee OA during stair negotiation. 84 Therefore, the effectiveness of the observed speed reduction ^{4,22} and changes in stepping 85 strategy in controlling knee joint loading during stair negotiation is unexplored. 86

The first objective of this study was to compare knee joint loading and trunk kinematics during stair ascent and descent in individuals with medial knee OA against healthy subjects during step-over-step at controlled speed. We hypothesize that OA patients will present lower knee loading than healthy subjects trying to avoid pain. The second objective was to investigate the influence of stair negotiation strategy on knee joint loading magnitude and distribution when individuals performed step-over-step at their preferred speed or were using step-by-step.

- 93 We hypothesize that by reducing stair walking speed or by using step-by-step instead of step-
- 94 over-step, patients will reduce the KCF and redistribute the knee loading to avoid the
- 95 overloading of the involved compartment.

96 Methods

Five participants (2 females and 3 males) were recruited for this study via a volunteer 97 database diagnosed in clinical practice with symptomatic bilateral medial knee OA. Eight 98 participants (4 females and 4 males) were recruited on a volunteer basis from the university 99 context, who were asymptomatic and had no history of OA. Participants underwent magnetic 100 resonance imaging (MRI) and completed the Hip²⁹ and Knee³⁰ disability and Osteoarthritis 101 Outcome Score questionnaires (Table 1). The Research Ethics committee for Science & 102 Engineering at the Metropolitan Manchester University approved the study. Participants signed 103 104 the written informed consent form prior to participation.

Patients were classified as having mild (1) moderate (2) and severe (3) knee OA based 105 on pain complaints and three parameters observed on the MRI (Table 2): cartilage defect; bone 106 107 marrow lesion (BML); and presence of osteophytes. Cartilage was scored for partial and full thickness loss as a % of the surface area in which: 0 when none; 1 when < 15% of cartilage 108 loss; 2 when 15-75% of cartilage loss; 3 when >75% of cartilage loss in a region (medial, lateral 109 or patellofemoral). BML size was scored as follows: 0 when none; 1 when BML size <1 cm; 2 110 BML when size >1 cm; 3 when multiple BML. Presence of osteophytes was scored based on 111 their size as follow: 0 when no osteophytes; 1 when size < 5mm; 2 when size < 1cm; 3 when 112 > 1cm. All patients presented with bilateral medial knee OA classified as moderate to severe 113 by a consultant radiologist. 114

Motion analysis was performed while barefoot ascending and descending a staircase consisting of seven 17.2cm-height steps (Figure 1). A 10-camera 3D motion capture system (Vicon Motion Systems Inc, Los Angeles, CA, USA) synchronized with four force platforms (embedded in the middle of the staircase) recorded the 3D position of 34 reflective markers according to an extended lower-body plug-in-gait marker set protocol ³¹ at 100 Hz, and measured ground reaction forces at 1000 Hz (Kistler, Amherst, New York, United States). Ground reaction forces were filtered using a second order Butterworth low pass filter, with cut-off level at 30Hz, and marker trajectories using a smoothing spline with cut-off at 6Hz.

Six trials per condition were collected for ascending and descending for step-over-step at controlled speed, *i.e.* alternating feet per step (Figure 1) with cadence controlled by a metronome at 90 beats per minute, corresponding to the normal self-selected stair walking speed in healthy subjects ³². Furthermore, two alternative strategies were tested: step-over-step at self-selected speed; and step-by-step at self-selected speed, *i.e.* both feet per step (Figure 1). The use of the handrail was not allowed. For safety reasons, patients wore a harness during the data collection.

A multi-body knee model with 6 degrees of freedom for the tibiofemoral and patellofemoral joints and fourteen ligaments was used. <u>More details about the model can be</u> <u>seen in the supplementary material.</u> Development and validation of the knee model are detailed elsewhere ³³. The model included an elastic foundation formulation ³⁴ to compute cartilage contact pressures. This model was integrated into an existing lower extremity musculoskeletal model ³⁵ with 44 musculotendon units.

The lower extremity model was scaled to subject-specific segment lengths as determined 136 in a static calibration trial. The joint angles were computed using an inverse kinematics 137 algorithm. The concurrent optimization of muscle activations and kinematics (COMAK) 138 algorithm ^{33,36}, was used to compute the secondary tibiofemoral and patellofemoral kinematics, 139 140 muscle and ligament forces, and contact forces by minimizing the muscle volume weighted sum of squared muscle activations plus the net knee contact energy. The COMAK algorithm 141 modulates muscle excitations to track knee flexion, while secondary knee motions 142 (tibiofemoral translations and non-sagittal rotations) and patellofemoral kinematics evolve 143 naturally due to muscle, ligament, cartilage contact, and external loading. The secondary 144 tibiofemoral kinematics and patellofemoral kinematics are load-dependent as they evolve as a 145

function of muscle and ligament forces, and cartilage contact. Tibiofemoral and patellofemoral 146 cartilage contact pressures were computed using an elastic foundation model ³⁴ in which 147 pressure is assumed to be a function of the depth of penetration between contacting cartilage 148 surfaces. Depths of penetration for each triangle in a mesh were determined at each time step 149 using ray-casting techniques ³⁷. At each triangle of the tibia plateau, the contact pressure was 150 computed, in which cartilage was assumed to have an elastic modulus of 10 MPa, a Poisson's 151 ratio of 0.45, and a uniform thickness of 2 mm for each surface ³⁴. Subsequently, an inverse 152 dynamics algorithm computed the external joint moments. 153

154 The knee model performance has previously been validated. As kinematic validation, the predicted joint kinematics in the secondary degrees of freedom of the knee were validated 155 against joint kinematics measured using dynamic MRI and are reported in the study of Lenhart 156 et al.³³. As dynamic validation, the calculated KCF were compared with instrumented implant 157 data provided through the Grand Challenge Competition to Predict in vivo Knee Loads, a 158 subject-specific data set that allows researchers to validate muscle and contact forces estimated 159 in the knee. When comparing between the measured and calculated KCF, the joint contact load 160 prediction errors (root-mean-square (rms) error = 0.33 BW)^{36,38} were comparable to those (rms) 161 error = 0.26 BW) observed from a unique optimization approach, termed force-dependent 162 kinematics, introduced by the 2014 "Grand Challenge" winner ³⁹, and slightly better than those 163 that have been obtained using traditional optimization or forward dynamic simulations ^{40,41}. 164

165 Calculated KCF were normalized to body weight (BW) and moments to the product of 166 body weight and height (BW×Ht). All data were time normalized to the stance phase (*i.e.* from 167 initial contact to toe off collected from either of the four force plates).

KCF, moments and angles throughout the stance phase were averaged over all trials for each leg. Trunk angles were calculated relative to the ground reference frame. The highest peaks during the first and second half of the stance phase for stair ascent and descent

respectively, were determined for the total KCF, medial KCF, and lateral KCF. The highest 171 peak KFM, KAM were determined for all activities whereas peak knee rotation moment 172 (KRM) were only clear for step-over-step tasks while ascending. Furthermore, maximum 173 contact pressures in the medial tibial plateau were assessed at the instant of peak medial KCF. 174 Independent-samples *t*-test (SPSS Inc., v17.0) evaluated the significance (p < .050) of 175 the differences in peaks (tested for normality by Kolmogorov-Smirnov and Shapiro-Wilk) 176 177 between the two groups and paired-samples t-test between strategies (step-over-step at controlled versus self-selected speed, and step-over-step versus step-by-step) within each 178 179 group.

As maximum contact pressures did not show a normal distribution, the non-parametric Mann-Whitney-U test was used to evaluate the significance (p < .050) of the differences between the two groups. Wilcoxon matched-pair test (p < .050) tested the significance of the differences between strategies within each group.

184 **Results**

Age, body mass and height, and also speed did not differ significantly between the two subject groups (Table 1). The medial OA group had significantly more knee pain (p < .001) and significantly higher function limitations in activities of daily living (p < .001) than controls. Level of knee pain was highly correlated with function limitations (R > 0.87).

Peak medial KCF (1.86±0.54, p < .000) and lateral KCF (1.52±0.36, p = .015) were 189 190 significantly lower in individuals with OA compared to controls (2.51±0.28 and 2.24±0.81, respectively, medial and lateral KCF) during stair ascent (Figure 2). During stair descent, on 191 192 the other hand, no significant differences were observed between the two groups (S1 Figure and S1 Table). Maximum contact pressures were also lower in individuals with OA, during 193 stair ascent, however, not statistically significant (Table 4). Patients with OA exhibited more 194 similar pressures during stair ascent and stair descent, whereas control subjects clearly reduced 195 pressures from ascending to descending (Figure 4). 196

Individuals with OA exhibited significantly lower peak KFM during both stair ascent (0.050 ± 0.017 , p = .002) and descent (0.058 ± 0.018 , p = .022) compared to controls (0.070 ± 0.012 and 0.073 ± 0.015 , respectively, at stair ascent and descent). No significant differences in the peak KAM or KRM were observed between the two groups (S2 Figure and S2 Table).

Individuals with OA had higher trunk flexion angles $(24.45\pm3.76, p = 0.001 \text{ during stair})$ ascent) and tended to lean the trunk more towards the leading leg in the frontal plane $(2.76\pm1.38, p = 0.069 \text{ during stair ascent})$ throughout the stance phase compared to controls $(18.43 (3.74) \text{ and } 0.93 (2.82), \text{ respectively, trunk flexion and trunk lean angles during stair$ ascent) during both stair ascent and descent (Figure 3 and S3 Table). During stair descent, theOA group exhibited a larger variation between subjects in the trunk kinematics in the frontaland transversal planes, shown by the high standard deviations, compared to controls. In all planes of motion, kinematics of the hip, knee and ankle joints showed a similar pattern of
movement between the two groups during stair ascent and descent (S3 Figure and S4 Figure).

When changing speed, all subjects walked slower when they could walk at their preferred 211 speed in comparison with the controlled condition, however only significantly during stair 212 ascent. During stair ascent at decreased speed, the peak medial KCF (p = .024) and lateral KCF 213 decreased (p = .002) in individuals with OA (S6 Figure and S4 Table), whereas the opposite 214 was found for peak lateral KCF (p = .009) in healthy subjects (S5 Figure and S4 Table). During 215 stair descent, no significant differences in KCF were observed between step-over-step at 216 217 controlled and self-selected speed in healthy or OA groups. No differences were observed in terms of maximum contact pressures between step-over-step at controlled and self-selected 218 speed in both groups (Table 4). 219

With reduced speed, patients with OA maintained the increased trunk flexion and lean angles towards the leading leg during stair ascent. During stair descent, on the other hand, OA patients exhibited a smaller variation in the trunk kinematics in the frontal and transversal planes as the speed decreased (S5 Table).

When changing strategies from step-over-step to step-by-step, both controls and OA 224 significantly reduced the speed while ascending (p < .001 and p = .009, respectively) and 225 descending stairs (p < .001 and p = .008, respectively) (Table 3). Both controls (p = .016) and 226 OA (p = .040) exhibited significantly higher peak lateral KCF when using step-by-step instead 227 of step-over-step during stair descent. During stair ascent, however, individuals with knee OA 228 significantly increased the peak medial KCF (p = .008) when using step-by-step, whereas no 229 significant differences were seen in controls (S4 Table). By altering from step-over-step to 230 step-by-step, maximum contact pressures were not significantly different neither in controls or 231 patients with OA (Figure 4 and Table 4) during stair ascent. However, during stair descent 232

- 233 maximum contact pressures significantly decreased in patients with OA when using step-by-
- 234 step (p = .007).

to per period

236 Discussion

This study investigated knee joint loading in terms of magnitude of KCF and cartilage 237 pressures, during stair ascent and descent in individuals with medial knee OA. Using a 238 multibody musculoskeletal model, we showed that patients with OA exhibited reduced 239 tibiofemoral loading during stair ascent, but not stair descent. The reduced contact force during 240 ascent was achieved by increasing the trunk flexion angle, which reduced the knee flexion 241 242 moment and thus muscle forces compressing the joint. This strategy was not as effective in stair descent, where the trunk was more vertical, thus the knee flexion moment cannot be 243 244 modulated without large adjustments to trunk flexion that compromise stability on stairs. Furthermore, different strategies in stair negotiation, such as reduction in speed, and employing 245 step-by-step instead of step-over-step were shown to be effective in reducing the knee contact 246 loading. 247

Our results confirmed the hypothesis that OA patients would present lower KCF than 248 controls. During stair ascent, when asked to walk at controlled speed, which was significantly 249 higher than their preferred speed, the OA group could effectively reduce both peak medial and 250 lateral KCF compared to control subjects. This was possible by executing higher trunk flexion 251 and higher trunk lean towards the leading leg compared to controls. By positioning the centre 252 of mass further forwards and more towards the leading leg at a time where knee is considerably 253 flexed, which potentially induces elevated joint moments, OA patients direct the ground 254 reaction force vector closer to the knee joint centre and, therefore, they reduce the KFM 255 (significantly) and KAM. In addition, the increased trunk flexion decreases the demand on the 256 knee extensors, which generate the propulsion required during stair ascent. Previous studies 257 have also found reduced KFM ^{4,11} and increased trunk flexion ¹¹ during stair ascent ^{4,11} and 258 descent ⁴ in OA patients compared to controls. Despite the reduced KCF, OA patients still 259 reported significantly higher pain complaints compared to controls. Our study is therefore the 260

first to determine that the altered stair walking pattern used by patients with OA, more specific the higher trunk flexion and reduced KFM, effectively unloads the knee joint as reflected in the reduced compartmental KCF.

During stair descent, the compensatory mechanisms used by the OA group were less 264 effective in reducing the knee loading than during stair ascent, and reductions in peak medial 265 and lateral KCF were not statistically significant. Patients could not increase the trunk flexion 266 267 angles during stair descent as much as they did during stair ascent compared to a healthy control, probably due to fear of falling. During stair descent, the body has to adopt to a more 268 269 upright position to maintain balance and, therefore, by leaning the trunk too far forwards, patients could compromise their balance ⁴² and, ultimately fall. The inability to reduce KCF 270 during descent may explain why patients experience higher knee pain ⁴³ during stair descent 271 than ascent. 272

The second hypothesis that OA patients would be able to reduce the KCF by reducing 273 the speed or by using step-by-step instead of step-over-step strategy has been partially 274 confirmed. When subjects walked at their preferred speed, which was significantly slower than 275 that at controlled execution during stair ascent, individuals with OA significantly reduced 276 medial KCF compared to those occurring at controlled speed, whereas controls kept similar 277 KCF at the medial compartment. When forced to increase their speed, some OA patients felt 278 forced to lean and rotate their trunk more, resulting in a high variation between subjects in the 279 280 trunk kinematics in these two planes during stair descent. This shows that some patients felt forced to use another mechanism rather than increased trunk flexion to perform stair descent 281 when speed was enforced. This suggests that it is more effective for patients to reduce medial 282 compartment loading during stair descent by reducing the walking speed than by altering trunk 283 kinematics. During stair ascent, on the other hand, the changes in the trunk kinematics were 284 still effective for OA patients to reduce knee loading, even at a higher stair walking speed. In 285

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addition, speed reduction allowed OA patients to decrease maximum medial compartment
contact pressure. Thus, a reduction in speed together with changes in trunk kinematics are the
key strategies used to reduce the knee loading during stair ascent, and a reduction in speed is
even more important to reduce the medial knee loading during stair descent.

By changing the stepping strategy and performing step-by-step instead of step-over-step 290 during stair ascent, OA patients significantly increased the medial KCF, even at significantly 291 292 lower speeds. This resulted from the fact that performing step-by-step, body tends to adopt a straighter position. On the other hand, during stair descent, by performing step-by-step instead 293 294 of step-over-step, they significantly decreased the medial knee contact pressures. Similarly, Reid et al.²³ reported that in healthy subjects, step-by-step strategy was more efficient in 295 reducing the peak KFM when compared to step-over-step strategy during stair descent than 296 297 stair ascent. From our findings, it is suggested that, in OA patients, step-by-step is only 298 effective in reducing the medial knee loading during stair descent, but not during stair ascent.

The magnitude of KCF in healthy subjects in the present study was higher for stair ascent 299 than those from literature based on measured KCF in subjects with instrumented prosthesis 300 ^{44,45}. Our controls exhibited an averaged peak total KCF of 4.41 (0.78) BW and 4.20 (0.74) BW 301 for, respectively, stair ascent and descent, whereas Kutzner et al. ⁴⁴ reported averages of 3.16 302 BW and 3.46 BW for the peak resultant force. Similar results, ranged from 2.90 to 3.50 BW, 303 were reported by Heinlein et al. ⁴⁵. More similarly, our OA group exhibited peak KCF of 2.78 304 305 (0.62) BW and 3.29 (1.14) BW for stair ascent and descent, respectively. Previous simulation studies on healthy subjects and those having TKR during stair ascent, presented compressive 306 joint reaction forces up to 4.00 BW ⁴⁶. Differences might be due to several reasons: 307 instrumented implant studies report on patients having TKR and an altered gait pattern may 308 therefore be present; none of the mentioned studies report stair walking speed nor the step 309 height. 310

The findings of this study should be viewed in light of the following specific limitations. 311 We used a single generic knee model that was scaled to represent the anthropometry of the 312 subjects instead of considering the subject-specific articular geometries, including those of the 313 tibia plateau. Subject-specific articular geometries, muscle-tendon and ligaments properties 314 were not considered in our approach since there was no data available for the cohort studied. 315 Therefore, our model does not account for OA induced changes in the articular geometry, 316 317 thickness and mechanical properties of the cartilage or changes in the ligaments. Consequently, the reported differences in KCF and contact pressures only result from altered kinematic and 318 319 kinetic behavior. Bone deformities, ligament laxity or changes in cartilage induced by joint degeneration were not taken into account although they may affect the calculated contact 320 pressures. However, the effect of having a 2-mm constant cartilage thickness instead of a 321 variable thickness on tibiofemoral contact pressure during gait has been previously assessed 322 and showed limited effect on the observed peak contact pressure (about 4%)⁴⁷. Furthermore, 323 although the validation of the model has shown a good agreement between the calculated and 324 experimental kinematics and contact forces in healthy subjects and patients following total 325 knee replacement ³³, this validation cannot easily be extended to an OA population. Therefore, 326 this model might present specific limitations when used in patients with knee OA, especially 327 those known to present increased co-contraction (Kellgren-Lawrence score ≥ 2) resulting in an 328 underestimation of the joint loading ⁴⁸. In this model, the ligaments are represented as nonlinear 329 330 spring elements, one-dimensional discrete elements, rather than deformable 3D representations that account for spatial variations in strain. Instead, some wrapping surfaces were included to 331 improve wrapping around the bony structures but no ligament-ligament interactions were 332 incorporated. The thickness of the cartilage surface was assumed constant, which is a 333 simplification since cartilage thickness varies. This simplification might result in differences 334 in terms of contact pressures and contact areas ⁴⁹. Further, the knee model does not include 335

menisci, which are known to distribute pressure in the tibiofemoral joint. Therefore, the
absence of menisci might increase the peak contact pressures in the knee joint surface. Finally,
it is known that the definition of other lower limb joints influences knee kinematics as well ⁵⁰,
especially the ankle joint, for which only one degree of freedom was considered.

In conclusion, during stair ascent, OA patients could effectively reduce the knee joint 340 loading by reducing their speed, increasing the trunk flexion and lean the trunk more towards 341 342 the leading leg. However, during stair descent, changes in the trunk flexion and frontal lean were more limited and less effective, requiring reduced speed or even more increased trunk 343 344 rotation and lean to effectively reduce the peak medial KCF and the contact pressures on the tibia plateau. Furthermore, this study suggests that, in OA patients, step-over-step is more 345 effective in reducing the medial knee loading, particularly at reduced speed, during stair ascent, 346 while step-by-step is more effective during stair descent. Understanding how these 347 compensatory mechanisms work across the whole body can help underpin recommendations 348 on alternative strategies for avoiding overloading of other joints. 349

Licz

350 Author contributions

All authors take responsibility for the integrity of the work as a whole, including data and accuracy of the analysis. Design: S. Meireles, N. Reeves and I. Jonkers. Conception: S. Meireles, N.D. Reeves, R.K. Jones, C.R. Smith, and D.G. Thelen. All the authors contributed to the analysis and interpretation of the data, drafting of the article and final approval of the article.

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361 Competing interests

362 All authors declare no conflict of interest.

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Figure 1 - Marker set on a representative subject while ascending the staircase (left) and a representative scheme of the step-over step (above right) and step-by-step (below right) tasks.

428x318mm (72 x 72 DPI)



Figure 2 - Peak medial KCF (MKCF) and lateral KCF (LKCF), comparing the two groups of subjects while performing different tasks: step-over-step at controlled speed (SOS CS), step-over-step at self-speed (SOS SS) and step-by-step (SBS) while ascending or descending stairs. * indicates a significant difference between the groups.
□ indicates a significant difference between the task in which there is this indication and the task step-over-step while ascending stairs for the control group, whereas • is used to the OA group.

263x107mm (120 x 120 DPI)



Figure 3 - Trunk kinematics relative to the ground reference frame in the sagittal (left), frontal (middle) and transversal (right) plane for step-over-step while ascending (above) and descending (below) stairs at controlled speed during stance phase, comparing healthy subjects and individuals with medial knee OA.

347x191mm (120 x 120 DPI)



Figure 4 - Group-averaged contact pressure distributions (MPa) on the articular surfaces of medial tibial plateau at the time instant of the first peak medial KCF. To obtain these averaged contact pressure distribution maps, the average contact pressure was calculated for every triangle of the medial tibial surface mesh and presented on a representative surface model. Results are presented for step-over-step at controlled speed; step-over-step at self-selected speed and step-by-step, while ascending and descending stairs for the healthy group (on the left), and the medial knee OA group (on the right).

Table 1 - Characteristics of the groups: control and medial OA.

	Mear	n (SD)	p	
	Control	Medial OA	(Control <i>vs</i> OA)	
No. of subjects	8	5	-	
No. of limbs	16	10	-	
Age, <i>years</i>	51.0 (13.4)	52.8 (11.0)	.806	
Body mass, <i>kg</i>	74.1 (13.7)	83.8 (14.8)	.255	
Height, <i>m</i>	1.66 (0.10)	1.70 (0.11)	.489	
KOOS score, %	96.7 (6.0)	42.3 (7.7)	< .001	
KOOS pain score, %	96.5 (7.8)	41.1 (13.4)	< .001	
KOOS function score,	08 0 (2 0)	54 1(7 7)	< 001	
%	90.9 (Z.0)	J4. I(<i>I</i> . <i>I</i>)	<	
R	0.968	0.876		
HOOS score, %	98.2 (4.6)	92.8 (10.4)	.214	

Statistically significant differences (p < .050) between the two groups of subjects, evaluated by the independent *t*-test, are indicated in bold.

Function score indicates the level of function in activities of daily living (ADL).

R is the Person correlation coefficient between pain and function scores, in which 1 indicates a perfect correlation between the two parameters.

 Table 2 – OA classification based on MRI and X-ray.

	Cor	itrol	Medial OA		
	Lateral knee Medial		Lateral knee	Medial	
	joint	knee joint	joint	knee joint	
Cartilage score	0	0	0.6	1.8	
BML	0	0	0.3	2	
Osteophytes	0	0	1.2	1.6	
K&L score	0 2-3 (4 out of 5)			ut of 5)	

Table 3 – Stair walking speed during step-over-step at controlled speed (SOS CS) and at self-selected speed (SOS SS), and step-by-step (SBS) in patients with medial knee OA compared to controls.

			Mean (SD)		p			
			Control	Medial OA	(Control <i>vs</i> OA)		<i>p</i> (Control)	<i>р</i> (ОА)
, m/s		SOS CS	0.59 (0.02)	0.57 (0.04)	0.107	CS	006	024
	cending	SOS SS	0.53 (0.08)	0.49 (0.12)	0.364	SS	<u>.000</u>	<u>.031</u>
	As	SBS	0.36 (0.04)	0.38 (0.03)	0.203	SOS <i>vs</i> SBS	<u>< .001</u>	<u>.009</u>
Speed		SOS CS	0.60 (0.03)	0.56 (0.08)	0.154	CS	180	107
	scending	SOS SS	0.57 (0.09)	0.49 (0.11)	0.057	SS	. 100	. 107
	Des	SBS	0.34 (0.05)	0.36 (0.04)	0.303	SOS vs SBS	<u>< .001</u>	≤ .001

Statistically significant differences (ρ < .050) between the two groups of subjects,

evaluated by the independent *t*-test, are indicated in bold.

Statistically significant differences (p < .050) between strategies (CS vs SS, and SOS vs SBS) within each group of subjects, evaluated by the paired-sample *t*-test, are indicated in bold.

Table 4 – Maximum contact pressures (*MPa*) at the peak medial KCF (MKCF) comparing the two groups of subjects and *p*- values comparing activities into the groups.

		Mear	n	
		Control (16 legs)	Medial OA (10 legs)	(C0 vs OA)
SOS CS	Ascending	24.1 (12.1)	16.0 (6.1)	.092
505 C5	Descending	15.8 (5.6)	14.2 (4.6)	.598
SOS SS	Ascending	24.4 (11.7)	13.9 (4.6)	<u>.004</u>
	Descending	15.7 (7.1)	13.8 (4.6)	.317
	Ascending	24.4 (12.6)	14.7 (4.6)	<u>.035</u>
SBS	Descending	16.1 (5.9)	11.4 (3.3)	<u>.013</u>
nding	p (SOS SS vs SOS CS)	.717	.093	
Ascen	p (SOS SS vs SBS)	.877	.059	
nding	p (SOS SS vs SOS CS)	.959	.445	
Desce	p (SOS SS vs SBS)	.877	<u>.007</u>	

Statistically significant differences (p < .050) in maximum contact pressures between the two groups of subjects, evaluated by Mann-Whitney-U test, are indicated in bold.

Statistically significant differences (p < .050) in maximum contact pressures between strategies within each group of subjects, evaluated by Wilcoxon matched-pair test, are indicated in bold. SOS CS, SOS SS and SBS correspond to step-over-step at controlled and self-selected speed, and step-by-step, respectively.

PART I -Knee Model

The multibody knee model was developed from MRI images of the right knee from a 23 years old female subject (height = 1.65 m, mass = 61 kg) with no history of chronic knee pain, injury, or surgery.

Anatomical reference frame orientations were established for each bone using an automatic algorithm based on geometric and inertial properties of the 3D segments ^{1, 2}.

The tibiofemoral and patellofemoral joints were both modeled as 6 degree of freedom with deformable contact. The passive restraints of the knee joint are provided by the major knee ligaments and joint capsule, represented by 14 bundles of non-linear springs: superficial and deep medial collateral ligament (sMCL, dMCL), lateral collateral ligament (LCL), anteriomedial and posteriolateral anterior cruciate ligament (aACL, pACL), anteriolateral and posteriomedial posterior cruciate ligament (aPCL, pPCL), patellar tendon (PT), medial and lateral patellofemoral ligaments (MPFL, LPFL), popliteofibular ligament (PFL), posteriomedial capsule (pmCAP), the posterior capsule (CAP), and the iliotibial band (ITB). Each ligament bundle was represented by a discrete number of strands. Each strand was assumed as a non-linear stiffening spring at low strains ($\varepsilon < 0.06$), and having a linear stiffness at higher strains ³. The ligament elastic modulus was assumed to be 125 MPa ⁴.

Tibiofemoral and patellofemoral cartilage geometry were segmented from MRI images (Mimics Innovation Suite, Materialise, Belgium). Tibiofemoral and patellofemoral cartilage contact pressures (*p*) acting between articulating surfaces were computed using an elastic foundation model ⁵, in which pressure is assumed to be a function of the depth of penetration between contacting cartilage surfaces.

$$p = -\frac{(1-v)E}{(1+v)(1-2v)} \ln\left[1 - \frac{d}{h}\right], \ (1)$$

with two additional equations resulting from the equilibrium of pressures in pairs of contacting triangles, and the equivalence of the sum of the individual surface penetration depths to the total penetration depth:

$$p_1 = p_2$$
 (2)

$$d_1 + d_2 = d \quad (3)$$

where *E* is elastic modulus, *v* is Poisson's ratio, *d* is the penetration depth and *h* is the combined thickness of the two cartilage surfaces. The system of equations (Eqs 2 and 3) is solved for each pair of contacting triangles (subscripts) in the cartilage meshes given the E, v, and thickness of each cartilage geometry. Cartilage was assumed to have an elastic modulus of 5MPa ³, a Poisson's ratio of 0.45 ⁶ and represented by uniform cartilage thickness of 2mm over each surface (*i.e.* 4 mm total thickness).

The model included 44 musculotendon actuators spanning the right hip, knee and ankle ⁷.

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PART II - Comparison between control subjects and medial OA

S1 Figure - Total, medial and lateral knee contact forces (KCF) during step-over-step (SOS) at **controlled speed** while ascending (above) and descending stairs (below) comparing healthy subjects and individuals with medial knee OA. * indicates a significant difference between the groups.

S1 Table - Peak values of the total, medial and lateral KCF (×BW) during the stance phase of step-over-step at **controlled speed** (SOS CS), while ascending (ASC) and descending (DESC) stairs comparing between the control (C0) group and the medial OA (OA) group.

Total			Control	Medial OA	p
		(26)	(16 legs)	(10 legs)	(C0 vs OA)
		TKCF	4.49 (0.85)	3.17 (0.82)	<u>.001</u>
	P1	MKCF	2.51 (0.28)	1.86 (0.54)	<u>< .001</u>
ASC		LKCF	2.24 (0.81)	1.52 (0.36)	<u>.015</u>
100	P2	TKCF	2.82 (0.65)	2.65 (0.53)	.492
		MKCF	1.56 (0.62)	1.52 (0.35)	.868
		LKCF	1.39 (0.43)	1.26 (0.44)	.454
		TKCF	3.26 (0.81)	2.72 (0.75)	.104
	P1	MKCF	2.11 (0.57)	1.58 (0.41)	<u>.019</u>
DESC		LKCF	1.28 (0.36)	1.34 (0.42)	.682
		TKCF	4.33 (0.96)	3.43 (1.12)	<u>.038</u>
	P2	MKCF	2.44 (0.54)	1.98 (0.65)	.063
		LKCF	2.11 (0.72)	1.58 (0.58)	.062

Statistically significant differences (p < .050) are indicated in bold and calculated by paired-samples *t*-test. KCF are expressed as mean (SD (BW), where SD is standard deviation. P1 and P2 correspond, respectively, to first and second peak of the stance phase.

S2 Figure - Knee flexion (left), adduction (middle) and rotation (right) moments during step-over-step (SOS) at **controlled speed** while ascending (above) and descending stairs (below) comparing healthy subjects and individuals with medial knee OA. * indicates a significant difference between the groups.

2 Table – Peak values of the KFM, KAM and KRM (BW*Ht) during stance phase of step-over-step at **controlled speed** (SOS CS) while ascending (ASC) and descending stairs (DESC).

		Total	Control	Medial OA	p
		(26)	(16 legs)	(10 legs)	(C0 vs OA)
ASC		KAM	0.017 (0.009)	0.016 (0.008)	.805
	P1	KFM	0.070 (0.012)	0.050 (0.017)	<u>.002</u>
		KRM	-0.008 (0.006)	-0.006 (0.004)	.235
	P2	KRM	0.002 (0.003)	0.001 (0.003)	.633
DESC	P2	KAM	0.021 (0.008)	0.016 (0.007)	.119
		KFM	0.073 (0.015)	0.058 (0.018)	<u>.022</u>

Statistically significant differences (p < .050) are indicated in bold and calculated by paired-samples *t*-test. Knee moments are expressed as mean (SD (BW*Ht), where SD

is standard deviation. P1 and P2 correspond, respectively, to first and second peak of the stance phase.

S3 Figure - Hip, knee and ankle kinematics at the sagittal (left), frontal (middle) and transversal (right) planes of rotation for step-over-step (SOS) while ascending stairs at **controlled speed** during stance phase comparing healthy subjects and individuals with medial knee OA.

S4 Figure - Hip, knee and ankle kinematics at the sagittal (left), frontal (middle) and transversal (right) planes of rotation for step-over-step (SOS) while descending stairs at **controlled speed** during stance phase comparing subjects and individuals with medial knee OA.

S3 Table - Trunk extension and bending angles (in degrees), at the time instant

of the first peak MKCF during SOS at controlled speed.

		Control	Medial OA	-
		(16 legs)	(10 legs)	ρ
	Trunk Flexion	19 /2 (2 7/)	24 45 (2 76)	001
SOS CS	Angles	10.43 (3.74)	24.43 (3.70)	<u>.001</u>
Ascending	Trunk Lean	0 03 (2 82)	2 76 (1 38)	060
	Angles	0.93 (2.02)	2.70 (1.30)	.009
SOS CS	Trunk Flexion	8 08 (3 13)	10 80 (3 11)	166
Descending	Angles	0.90 (3.43)	10.09 (3.11)	. 100

Trunk Lean	0.00 (2.67)	0.70 (7.70)	760
Angles	0.09 (2.07)	0.73 (7.72)	.702

Statistically significances (p < .050) are indicated in bold and calculated by *t-test*.

Positive trunk flexion angles correspond to flexion of the trunk; positive trunk bending correspond to bending towards the leading leg.

SOS CS corresponds to step-over-step at controlled speed.

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PART III - Comparison between strategies: SOS at controlled versus self-selected speed and SOS versus SBS

S5 Figure - Total, medial and lateral knee contact forces (KCF) in **healthy subjects** comparing step-over-step at controlled speed (SOS CS) and step-over-step at self-selected speed (SOS SS) while ascending (above) and descending (below) stairs. * indicates a significant difference between the two tasks.

S6 Figure - Total, medial and lateral knee contact forces (KCF) in individuals with medial knee OA comparing step-over-step at self-selected speed (SOS SS) and stepover-step at controlled speed (SOS CS) while ascending (above) and descending (below) stairs. * indicates a significant difference between the two tasks.

S4 Table - Peak values of the total, medial and lateral KCF (×BW) during the stance phase of step-over-step at controlled speed (SOS CS), step-over-step at self-selected speed (SOS SS) and step-by-step (SBS) while ascending and descending stairs for the control and medial OA groups comparing between tasks.

	ASCENDING				DESCENDING						
		SOS CS	SOS SS	SBS	p CS vs SS)	p (SS vs SBS)	SOS CS	SOS SS	SBS	p (CS vs SS)	p (SS vs SBS)
CONTROL	TKCF	4.49 (0.85)	4.41 (0.78)	4.56 (0.86)	.414	.182	4.33 (0.96)	4.20 (0.74)	4.44 (0.73)	.473	.087
	MKCF	2.51 (0.28)	2.61 (0.26)	2.64 (0.34)	.190	.672	2.44 (0.54)	2.44 (0.43)	2.43 (0.35)	.977	.797
	LKCF	2.24 (0.81)	2.04 (0.67)	2.17 (0.69)	<u>.009</u>	.066	2.11 (0.72)	1.92 (0.53)	2.31 (0.60)	.144	<u>.016</u>
MEDIAL OA	TKCF	3.17 (0.82)	2.78 (0.62)	2.94 (0.70)	<u>.007</u>	.101	3.43 (1.12)	3.29 (1.14)	3.48 (1.03)	.506	.215
	MKCF	1.86 (0.54)	1.64 (0.45)	1.81 (0.40)	<u>.024</u>	<u>.008</u>	1.98 (0.65)	1.90 (0.58)	1.95 (0.50)	.547	.657
	LKCF	1.52 (0.36)	1.32 (0.29)	1.36 (0.31)	<u>.002</u>	.425	1.58 (0.58)	1.52 (0.72)	1.73 (0.74)	.628	<u>.040</u>

Statistically significant differences (p < .050) are indicated in bold and evaluated by the paired-sample t-test. KCF are expressed as mean (SD (BW), where SD is standard deviation. KCF corresponding to the peak KCF of the different tasks, i.e., first and second peaks KCF for ascending and descending, respectively.

S5 Table - Trunk extension and bending angles (in degrees), at the time instant of the first peak medial KCF during SOS while ascending and descending stairs for the control and medial OA groups comparing between controlled and self-selected speed.

			ASCENDING		DESCENDING			
		SOS CS	SOS SS	p (CS vs SS)	SOS CS	SOS SS	p (CS vs SS)	
CONTROL	Trunk Flexion	18.43	18.10	.331	8.98	0.00	.753	
		(3.74)	(3.26)		(3.43)	(9.29)		
	Trunk Lean	0.93	0.83	<u>.004</u>	0.09	-1.00	.254	
		(2.82)	(2.92)		(2.67)	(2.42)		
MEDIAL OA	Trunk Flexion	24.45	23.71	304	10.89	11.50	157	
		(3.76)	(3.31)	.504	(3.11)	(3.64)	.157	
	Trunk Lean	2.76	3.06	.602	0.73	0.57	.942	
		(1.38)	(2.14)		(7.72)	(2.01)		

Statistically significant differences (p < .050) in the trunk angles between strategies within each group of subjects, evaluated by the paired-sample *t*-test, are indicated in bold. Angles are expressed as mean (SD (°), where SD is standard deviation.



149x91mm (96 x 96 DPI)



159x83mm (96 x 96 DPI)



150x79mm (96 x 96 DPI)



153x78mm (96 x 96 DPI)



159x92mm (96 x 96 DPI)



158x95mm (96 x 96 DPI)