

1 **Biomechanical responses to changes in friction on a clay court surface**

## 1           **1. Abstract**

2    *Objectives:* To examine the influence of clay court frictional properties on tennis players'  
3    biomechanical response.

4    *Design:* Repeated measures

5    *Methods:* Lower limb kinematic and force data were collected on sixteen university tennis  
6    players during 10 x 180° turns (running approach speed  $3.9 \pm 0.20 \text{ m}\cdot\text{s}^{-1}$ ) on a synthetic clay  
7    surface of varying friction levels. To adjust friction levels the volume of sand infill above the  
8    force plate was altered (kg per  $\text{m}^2$  surface area; 12, 16 and  $20 \text{ kg}\cdot\text{m}^{-2}$ ). Repeated measures  
9    ANOVA and Bonferroni's corrected alpha post-hoc analyses were conducted to identify  
10   significant differences in lower limb biomechanics between friction levels.

11   *Results:* Greater sliding distances ( $\eta_p^2 = 0.355$ ,  $p = 0.008$ ) were observed for the lowest friction  
12   condition ( $20 \text{ kg}\cdot\text{m}^{-2}$ ) compared to the 12 and  $16 \text{ kg}\cdot\text{m}^{-2}$  conditions. No differences in ankle joint  
13   kinematics and knee flexion angles were observed. Later peak knee flexion occurred on the  
14    $20 \text{ kg}\cdot\text{m}^{-2}$  condition compared to the  $12 \text{ kg}\cdot\text{m}^{-2}$  ( $\eta_p^2 = 0.270$ ,  $p = 0.023$ ). Lower vertical ( $\eta_p^2 =$   
15    $0.345$ ,  $p = 0.027$ ) and shear ( $\eta_p^2 = 0.396$ ,  $p = 0.016$ ) loading rates occurred for the  $20 \text{ kg}\cdot\text{m}^2$   
16   condition compared to the  $16 \text{ kg}\cdot\text{m}^2$ .

17   *Conclusions:* Lower loading rates and greater sliding distances when clay surface friction was  
18   reduced suggests load was more evenly distributed over time reducing players' injury risks.  
19   The greater sliding distances reported were accompanied with later occurrence of peak knee  
20   flexion, suggesting longer time spent braking and a greater requirement for muscular control  
21   increasing the likelihood of fatigue.

22   **Keywords:** Kinematics; loading rate; sliding; lower limb; injury risks

## 2. Introduction

Tennis court surfaces differ greatly in mechanical properties, particularly in those influencing friction.<sup>1-3</sup> Tennis players must adapt to the varied mechanical properties throughout a season, which can influence player movements and loading.<sup>4,5</sup> Strategies previously suggested to reduce potentially high loading on high friction surfaces have included longer braking time, greater delayed peak knee flexion and altered pressure distribution patterns.<sup>4,6,7</sup> It has been suggested that players' ability to slide on lower friction clay surfaces has resulted in lower loading and therefore reduced injury risks.<sup>4,5,7</sup>

Different playing styles reported between acrylic and clay courts have also been attributed differences in frictional properties of the surfaces.<sup>8</sup> Longer rally lengths, greater player distances covered and greater proportion of baseline points on clay courts have been suggested to lead to greater physiological responses such as increased heart rate and blood lactate.<sup>9,10</sup> However, when duration of rally, proportion of baseline shots and distances covered were maintained, greater physiological response was still apparent on a clay court compared to an acrylic court.<sup>11</sup> Altered movement patterns such as sliding during rapid decelerations or changes in direction on clay court surfaces allows players to reposition quicker following a tennis shot.<sup>12</sup> Sliding has also been associated with increased muscle activity<sup>13</sup>, which could provide some explanation to the greater physiological response observed when duration and distance are comparable.

On low friction surfaces, such as clay, it is not unusual to observe players sliding during rapid decelerations such as during changes in direction.<sup>3</sup> Tennis players have been reported to utilise greater shear forces and shear loading rates in order to increase utilised coefficient of friction (COF), allowing for sliding to occur on clay surfaces.<sup>4</sup> Furthermore, sliding on clay surfaces have been reported to result in greater ankle inversion angles and lower initial knee flexion angles,<sup>4</sup> which are associated with ankle inversion injuries and ACL injuries respectively.<sup>14,15</sup> However, the authors suggested that although ankle and knee orientation

1 suggests players were more at risk on a clay surface compared to an acrylic, the lower  
2 mechanical friction properties on the clay would minimise risk of sudden stopping and  
3 overloading of the joints.<sup>4</sup>

4 The COF on clay courts can vary between 0.5 and 0.7;<sup>2</sup> as a result of differences in infill  
5 properties such as volume of infill, the degree of saturation and infill particle size.<sup>1,16</sup> Previous  
6 studies have examined the biomechanical differences between acrylic and clay courts which  
7 have distinctly different frictional properties.<sup>4,5,7</sup> Yet, there is a lack of evidence regarding  
8 tennis players' biomechanical response to small changes in friction, occurring between and  
9 within clay courts, and the implications these may have upon performance or injury risks.  
10 Therefore the current study aims to examine the influence of changes in frictional properties  
11 of a clay surface on biomechanical response. From the literature evidence, it is hypothesised  
12 that the level of friction will influence the tennis players' response such that as friction is  
13 reduced, greater shear forces ( $H_1$ ) and shear loading rates ( $H_2$ ) will occur. Reduced friction is  
14 hypothesised to result in lower initial knee flexion ( $H_3$ ) and delayed peak knee flexion ( $H_4$ ). At  
15 the ankle, it is hypothesised that ankle inversion angle will increase as a result of reduced  
16 mechanical friction ( $H_5$ ). There is no evidence to suggest changes in sagittal plane ankle  
17 movement will occur ( $H_6$ ) when friction is reduced on the clay surface.

### 18 **3. Methods**

19 Sixteen university tennis players (age  $19.93 \pm 0.96$  years, mass  $66.75 \pm 10.36$  kg, height  $1.74$   
20  $\pm 0.10$  m, and LTA rating  $7.48 \pm 2.18$ ) volunteered for the present study. All participants were  
21 free from injury and trained regularly (at least once a week) on acrylic courts. Players reported  
22 that they had minimal experience of playing on clay courts (i.e. playing on clay once a year or  
23 less). The study was approved by the Institutional Ethics Committee. Informed consent and  
24 physical activity readiness questionnaire results were obtained before any testing occurred.

1 A 9 m runway, which consisted of a synthetic clay surface, comprising of a carpet base layer  
2 (a dense, red, polypropylene fibrillated surface) and a top layer with a red granulate infill,<sup>1</sup> was  
3 used in a laboratory setting during the present study. In the area where participants were  
4 turning (above the force plate), the frictional conditions were altered through the use of  
5 different volumes of sand (Table 1). To enable ease of preparing the infill a removable square  
6 of the synthetic clay surface was placed over the force plate and was secured using Velcro®  
7 to enable quick removal of the sand and to ensure no movement of the synthetic clay surface  
8 during data collection. The three levels of friction were achieved using 12 kg.m<sup>-2</sup> (as  
9 recommended by the manufacturers), 16 kg.m<sup>-2</sup> and 20 kg.m<sup>-2</sup> of sand infill. Differences in  
10 mechanical friction were determined using a traction test device<sup>16</sup> and provided surface  
11 conditions which were within ITF regulations.<sup>17</sup> The traction test device replicated sliding on  
12 clay with the forefoot of a clay court shoe set at 7° against the surface and 90° against the  
13 direction of movement). Static and dynamic COF were recorded for a range of normal forces  
14 (1000 – 1600 N) which were selected based on data from previous research examining tennis-  
15 specific skills.<sup>4</sup> Static COF was defined as the peak COF indicating the transition between the  
16 static and dynamic regimes. The dynamic COF was taken as the average COF following the  
17 peak COF measured between 0.05 m and 0.20 m. Further details on the traction device and  
18 methods used to determine the conditions are reported by Clarke et al.<sup>1</sup> and Ura et al.<sup>16</sup>

19 \*\*\*\*Table 1 near here\*\*\*\*

20 Prior to each trial the infill sand on the area of interest (force plate) was removed, the sand for  
21 the next condition was then weighed and placed on the area of interest and spread evenly.  
22 During all testing participants wore the same tennis shoe model (Adidas Barricade 6.0 clay  
23 shoes). Ten successful 180° turning movements were performed, without a tennis racket, for  
24 each condition in a random order. Participants approached the turn at  $3.9 \pm 0.20$  m.s<sup>-1</sup>, which  
25 was assessed using timing gates set 2.3 m apart and 1.2 m from the force plate. Participants  
26 were asked to perform each 180° turn with their dominant leg (i.e. forehand side) and turn as

1 efficiently as possible. Each turn was performed on the force plate (with the required friction  
2 condition).

3 Three-dimensional lower limb kinematic data (120 Hz) were collected to examine ankle and  
4 knee movement. Data were collected using a passive marker motion capture system  
5 consisting of eight cameras (opto-electronic system; Peak Performance Technologies, Inc.,  
6 Englewood, CO), placed in an oval shape around the force plate. Eleven lower limb markers  
7 (greater trochanter, medial and lateral femoral epicondyle, anterior aspect of shank, proximal  
8 and distal bisection of posterior shank, proximal and distal bisection of the calcaneus, lateral  
9 malleolus, base of 2<sup>nd</sup> metatarsal and 5<sup>th</sup> metatarsal phalange) on the turning leg were used  
10 to construct joint coordinate systems with a custom written Matlab code (Matlab, R2011b,  
11 MathsWorks, Natick, MA, USA). A quintic spline filter was applied to the raw data (Peak  
12 Performance default optimal smoothing technique using 5<sup>th</sup> degree quintic polynomials). All  
13 kinematic data were presented relative to a relaxed standing trial. Initial and peak angles for  
14 sagittal plane ankle and knee rotations, and frontal plane ankle rotations were obtained.  
15 Occurrence times of peak angles were reported relative to initial foot contact. Relative  
16 occurrence times were also obtained and expressed as a percentage of contact time.

17 Sliding was determined using the velocity of centre of the foot (determined from the distal  
18 calcaneus marker and 2<sup>nd</sup> metatarsal marker). A sliding phase was determined when the  
19 velocity was greater than a threshold of 1 mm.s<sup>-1</sup> and maintained for more than 10 ms. During  
20 this sliding phase, sliding distance was determined by the resultant distance covered by the  
21 centre of the foot.

22 Ground reaction forces were measured at 960 Hz using an AMTI force plate (Advanced  
23 Mechanical Technology, Inc, Newton, MA). Vertical force parameters included peak impact  
24 force, peak active force, average loading rate and peak loading rate. Shear forces (FShear)  
25 were calculated as the resultant force of the anterior-posterior (Fy) and medio-lateral forces  
26 (Fx). Shear force parameters included peak shear force magnitude and loading rate. The

1 utilised COF was determined as the ratio between the shear force ( $F_{\text{shear}}$ ) and the vertical  
2 force ( $F_z$ ). Peak utilised COF, suggested to indicate the transition between the static and  
3 dynamic regimes,<sup>1</sup> was determined as the maximum COF value. Examples of the force data,  
4 utilised COF and sliding distance are demonstrated in Figure 1.

5 \*\*\*\*Figure 1 near here\*\*\*\*

6 An ANOVA with repeated measures (SPSS v.11) was conducted to examine tennis players'  
7 biomechanical response to the different friction conditions. Bonferroni's corrected alpha post-  
8 hoc analyses were applied to establish where differences occurred. An alpha level of 0.05 was  
9 used to identify any significant differences. Standardised effect sizes were calculated using  
10 partial  $\eta^2$  ( $\eta_p^2$ ) to provide the degree to which any differences were present.

#### 11 **4. Results**

12 Friction was a contributing factor that influenced the sliding distances achieved ( $\eta_p^2 = 0.355$ ,  
13  $p = 0.008$ ). For instance, the lowest level of friction ( $20 \text{ kg}\cdot\text{m}^{-2}$ ;  $0.23 \pm 0.16 \text{ m}$ ) produced  
14 significantly greater sliding distance compared to the  $16 \text{ kg}\cdot\text{m}^{-2}$  ( $0.17 \pm 0.12 \text{ m}$ ) and  $12 \text{ kg}\cdot\text{m}^{-2}$   
15 ( $0.18 \pm 0.13 \text{ m}$ ) conditions which had greater mechanical friction.

16 The analysis revealed no differences in the initial and peak knee angle between the three  
17 friction conditions (Table 2). However, friction level was found to have a significant influence  
18 on the occurrence time of peak knee flexion ( $\eta_p^2 = 0.270$ ,  $p = 0.023$ ). Post hoc analysis  
19 revealed that the  $20 \text{ kg}\cdot\text{m}^{-2}$  condition ( $0.34 \pm 0.09 \text{ s}$ ) resulted in a later peak knee flexion than  
20 observed for the  $12 \text{ kg}\cdot\text{m}^{-2}$  condition ( $0.31 \pm 0.07 \text{ s}$ ). When represented as a percentage of  
21 contact time, the relative occurrence of peak knee flexion were similar between conditions. As  
22 presented in Table 2, no differences in ankle movement were reported between the friction  
23 conditions.

1 \*\*\*\*Table 2 near here\*\*\*\*

2 The analysis revealed no significant differences in peak impact force, peak active force and  
3 peak shear force between the three friction conditions (Table 2). Peak vertical loading rate  
4 was significantly lower during the 20 kg.m<sup>-2</sup> condition ( $135.52 \pm 23.16$  BW/s;  $\eta_p^2 = 0.345$ ,  $p =$   
5  $0.027$ ) compared to the 16 kg.m<sup>-2</sup> condition ( $147.67 \pm 25.77$  BW/s). Friction level significantly  
6 influenced peak shear loading rate ( $\eta_p^2 = 0.396$ ,  $p = 0.016$ ), with lower shear loading rates  
7 produced during the 20 kg.m<sup>-2</sup> condition ( $53.25 \pm 10.45$  BW/s) compared to the 16 kg.m<sup>-2</sup>  
8 condition ( $58.78 \pm 10.92$  BW/s). The occurrence time of peak utilised COF was later for 20  
9 kg.m<sup>-2</sup> friction level ( $0.043 \pm 0.004$  s;  $\eta_p^2 = 0.306$ ,  $p = 0.040$ ) compared to the 16 kg.m<sup>-2</sup> friction  
10 level ( $0.037 \pm 0.003$  s). However, the magnitude of the peak utilised COF was similar between  
11 the three conditions.

## 12 5. Discussion

13 Sliding on clay is a common feature of tennis,<sup>3</sup> where players aim to initiate sliding in a timely  
14 manner to enable a quick change of direction.<sup>12</sup> In the current study, greater sliding distances,  
15 reduced loading rates and later peak knee flexions were achieved when friction was reduced.  
16 These findings suggest loading was more evenly distributed over time when clay court surface  
17 friction was reduced. In addition, greater sliding distances and later peak knee flexion suggest  
18 longer time was spent controlling the slide when friction was reduced, which could increase  
19 the likelihood of fatigue.

20 Sliding occurs when the shear force applied is greater than the static friction force.<sup>1,4</sup> Previous  
21 reports have identified higher shear forces on low friction clay surfaces compared to a high  
22 friction acrylic surfaces, which resulted in increased utilised COF leading to players sliding on  
23 the clay court.<sup>4</sup> However, the present study reported no differences in shear forces and peak  
24 utilised COF between the different friction conditions on the clay surface. These different



1 results are most likely due to differences in player movement mechanics on different court  
2 surface types. In previous work, Damm et al.<sup>4</sup> examined two distinct levels of friction (acrylic  
3 and clay surfaces), resulting in differences in the utilisation of friction. For example, when on  
4 the acrylic surface participants reduced their shear loading to reduce coefficient of friction,  
5 possibly reducing injury risks associated with loading on high friction surfaces.<sup>4</sup> Whilst, on the  
6 clay court the greater shear forces would enable participants to overcome the static friction  
7 and initiate sliding.<sup>1,4</sup> However, the present study focused on clay surfaces where participants  
8 were able to slide during all conditions. With no differences in shear force observed across  
9 the three surface friction levels, the lower friction surfaces allowed greater sliding distances  
10 owing to a lower resistance to sliding (lower mechanical COF).

11 Sliding reported for the lowest friction condition resulted in reduced shear and vertical loading  
12 rates compared to the 16 kg.m<sup>-2</sup>. The lower rate of loading on the lower friction surface as a  
13 result of further sliding suggests a reduced risk of injury by increasing the time spent applying  
14 the shear and vertical loads.<sup>18</sup> Reduced mechanical friction reduces the initial shear stiffness  
15 of the surface, i.e. lower resistance to movement or sliding, therefore reducing the load  
16 experienced by the players during impact<sup>1</sup> The reduced loading rate reported in the current  
17 study occurred in conjunction with later occurrence of peak knee flexion. Longer braking  
18 phases, through later peak knee flexion, have previously been suggested to result in reduced  
19 loading to accommodate the potential high loading when turning on high friction surfaces,  
20 therefore reducing the risk of injury.<sup>6</sup> However, findings in the current study suggest later peak  
21 knee flexion, and thus later braking occurred on the lower friction clay condition rather than for  
22 the higher friction clay conditions. It is important to note that the surfaces reported in the Durá  
23 et al.<sup>6</sup> study had a greater range of mechanical friction (0.43 - 0.93) which span those  
24 previously observed for clay and acrylic courts<sup>2</sup>. However, the present study focused on low  
25 friction levels on a clay surface where the coefficient of friction ranged between 0.54 - 0.63,  
26 similar to that previously reported for clay court surfaces<sup>2</sup>. Marked differences in friction (acrylic  
27 and clay) have previously resulted in distinct differences in technique and pressure

1 distributions to enable sliding on clay.<sup>4,7,19</sup> This may explain the contrasting results with those  
2 of Durá et al.<sup>6</sup> The present study reported players sliding for all conditions, which was not  
3 reported by Durá et al.<sup>6</sup> When occurrence time was represented relative to contact time, no  
4 differences between conditions were reported. These findings suggest that a similar technique  
5 was used, but sliding increased the total time of the step.

6 Sliding movements in tennis have been demonstrated to require greater muscular control  
7 compared to regular footwork.<sup>13</sup> Greater sliding distances and later peak knee flexions  
8 reported in the current study are likely to be associated with longer eccentric muscle  
9 contractions in order to control the movement, which is likely to increase physiological  
10 demands, such as increased heart rate and blood lactate accumulation. These findings  
11 suggest that reductions of friction below the manufacturer's recommendations could increase  
12 the physiological demand placed on players and therefore increase the likelihood of fatigue.  
13 Therefore, on surfaces such as clay that result in longer rally lengths and permit sliding,  
14 players could experience even greater increases in physiological strain, therefore increasing  
15 the likelihood of fatigue. Fatigue in tennis has been associated with reduced performance<sup>20,21</sup>  
16 and increased risk of injury.<sup>22,23</sup>

17 It must be noted that the current study was undertaken within laboratory conditions which  
18 limited the movements analysed, therefore reducing the ecological validity of the data.  
19 However, the turning movement was selected to reproduce a typical movement seen in tennis.  
20 The composition of the synthetic clay surface (carpeted base layer and red granulated infill)  
21 used in the current study differs to outdoor clay courts. Mechanical properties of these  
22 surfaces may differ and therefore alter players' response. However, the current study provides  
23 an insight to players' response to changes in friction on a surface that permits sliding.

## 6. Conclusions

Sliding is an influencing factor in players' response when examining clay court surface friction. Contrary to the study hypothesis, the current study did not report changes in shear force magnitudes ( $H_1$ ), whilst shear force loading rates were reduced as friction decreased ( $H_2$ ). Greater sliding distances accompanied by reduced shear loading rates on the lower friction conditions suggests reduced injury risks. In contrast to the study's hypothesis, no differences in knee flexion angles ( $H_3$ ) and ankle inversion angles ( $H_5$ ) were identified. Sagittal plane ankle kinematics remained similar between friction conditions ( $H_6$ ), as expected. As hypothesised, later knee flexion ( $H_4$ ) was observed during the lower friction conditions when greater sliding distances were also observed. Although sliding on clay enables efficient changes of direction and reduces injury risks through lower forces and longer time applying these forces, the current study's findings suggest that prolonged sliding on clay surfaces with low shoe-surface friction may lead to greater physiological strain. Therefore, it is important to maintain the manufacturer recommendations for infill volume, between and within matches, to limit excessive physiological strain due to greater sliding whilst still allowing players to benefit from sliding on the low friction surfaces.

## 7. Practical implications

- Clay court frictional properties influence player movement and loading during sliding, likely affecting injury risks and physiological responses
- It is important to maintain manufacturer recommendations for infill volume, between and within matches, to allow the benefits observed from sliding to be maintained but limit the physiological strain associated with lower friction surfaces

1           **8. Acknowledgements**

2    The authors would like to thank the International Tennis Federation for their support during  
3    the study.

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1        **10. Tables and captions**

2        **Table 1: Range of static coefficient of friction (COF) during a range of normal forces**  
3        **(1000N – 1600N) for three volumes of sand infill**

<b>COF</b>	
12 kg.m <sup>-2</sup>	0.61 - 0.64
16 kg.m <sup>-2</sup>	0.59 - 0.65
20 kg.m <sup>-2</sup>	0.54 – 0.59

4



1 **Table 2: Means and standard deviations for kinematic and kinetic data collected for**  
 2 **each friction condition**

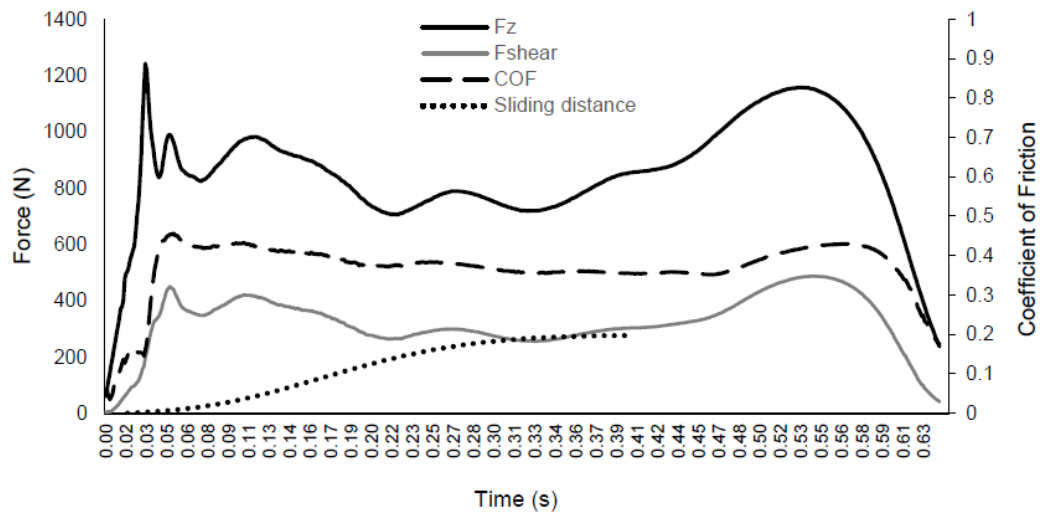
<b>Variable</b>	<b>12 kg.m<sup>-2</sup></b>	<b>16 kg.m<sup>-2</sup></b>	<b>20 kg.m<sup>-2</sup></b>
<i>Kinematic data</i>			
Knee flexion angle			
At impact (°)	17.3 ± 13.6	13.6 ± 13.6	16.5 ± 12.0
Peak (°)	40.0 ± 5.2	39.5 ± 5.7	39.6 ± 6.2
Time of peak (s)	0.31 ± 0.07	0.30 ± 0.07	0.34 ± 0.09*
Relative time of peak (%)	53.44 ± 9.81	51.94 ± 9.20	57.46 ± 9.92
Ankle flexion angle			
At impact (°)	4.4 ± 12.6	3.0 ± 11.3	4.6 ± 12.0
Peak (°)	-12.2 ± 7.3	-10.9 ± 8.9	-12.3 ± 7.4
Time of peak (s)	0.26 ± 0.12	0.19 ± 0.12	0.22 ± 0.12
Relative time of peak (%)	53.32 ± 7.10	53.41 ± 7.38	50.37 ± 6.19
Ankle inversion angle			
At impact (°)	-4.6 ± 17.2	2.2 ± 13.3	-2.8 ± 17.0
Peak (°)	-30.4 ± 8.5	-29.3 ± 7.5	-27.9 ± 8.7
Time of peak (s)	0.24 ± 0.09	0.23 ± 0.08	0.19 ± 0.08
Relative time of peak (%)	49.72 ± 8.00	48.03 ± 8.40	45.60 ± 8.67
<i>Kinetic data</i>			
Peak impact force (BW)	1.80 ± 0.49	1.92 ± 0.55	1.90 ± 0.50
Peak active force (BW)	1.32 ± 0.24	1.33 ± 0.88	1.28 ± 0.27
Peak shear force (BW)	0.76 ± 0.28	0.81 ± 0.23	0.78 ± 0.22
Average loading rate (BW/s)	37.75 ± 19.31	42.19 ± 21.18	41.67 ± 19.78
Peak vertical loading rate (BW/s)	140.22 ± 87.74	147.67 ± 25.77**	135.52 ± 23.16
Horizontal peak loading rate (BW/s)	54.94 ± 26.84	58.78 ± 10.92**	53.25 ± 10.45
Peak utilised COF	0.62 ± 0.13	0.55 ± 0.08	0.53 ± 0.14
Time of peak utilised COF (s)	0.035 ± 0.002	0.040 ± 0.003**	0.043 ± 0.004

3 \*denotes a significant difference with the 12 kg.m<sup>-2</sup>condition, \*\* denotes a significant difference with the 20  
 4 kg.m<sup>-2</sup>condition

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## 11. Figure and captions



**Figure 1: Examples of vertical ( $F_z$ ) and shear ( $F_{\text{shear}}$ ) ground reaction forces, utilised coefficient of friction (COF) and associated sliding distance for one subject during the turning movement**

2