1	Local Dynamic Stability of the Locomotion of Lower Extremity Joints and Trunk
2	Segment during Backward Upslope Walking
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4	Yu Wu ^{1, 2, 3} , Anmin Liu ⁴ , Ke-Rong Dai ^{1, 2, 3} , Dong-Yun Gu ^{1, 2, 3, *}
5	¹ Department of Orthopedic Surgery & Shanghai Key Laboratory of Orthopaedic
6	Implant, Shanghai Ninth People's Hospital of Shanghai Jiao Tong University, Shanghai,
7	China.
8	² Biomedical Engineering School of Shanghai Jiao Tong University, Shanghai, China.
9	³ Engineering Research Center of Digital Medicine and Clinical Translation, Ministry
10	of Education of P.R.China, Shanghai, China.
11	⁴ School of Health Sciences, University of Salford, Manchester, United Kingdom.
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15	Correspondence Address:
16	Dong-Yun Gu, PhD
17	Shanghai Ninth People's Hospital, Shanghai Jiao Tong University, 639 Zhizaoju Rd.,
18	200011, Shanghai, China
19	Tel: 86-21-23271133, Fax: 86-21-63137020, E-mail address: dongyungu@sjtu.edu.cn
20	
21	Running Title: Gait stability during backward upslope walking

22 ABSTRACT

Backward slope walking was considered as a practical rehabilitation and training
skill. However, its gait stability has been hardly studied, resulting in its limited
application as a rehabilitation tool.

In this study the effect of walking direction and slope grade were investigated on the local dynamic stability of the motion of lower extremity joints and trunk segment during backward and forward upslope walking (BUW/FUW). The local divergence exponents (λ_s) of 16 adults were calculated during their BUW and FUW at grades of 0%, 5%, 10%, and 15%. Mean standard deviation over strides (MeanSD) was analyzed as their gait variability.

Backward walking showed larger λ_S for the abduction-adduction and rotational angles of knee and ankle on inclined surface than forward walking, while λ_S for hip flexion-extension angle at steeper grades was opposite. No grade effect for any joint existed during BUW, while λ_S increased with the increasing grade during FUW. As to the trunk, walking direction did little impact on λ_S . Still, significant larger λ_S for its medial-lateral and vertical motion were found at the steeper grades during both FUW and BUW.

Results indicate that during BUW, the backward direction may influence the stability of joint motions, while the trunk stability was challenged by the increasing grades. Therefore, BUW may be a training tool for the stability of both upper and lower body motion during gait.

Keywords: Backward slope walking, Local dynamic stability, Local divergence
exponent, Gait analysis

INTRODUCTION

Backward slope walking (BSW), including backward upslope and backward 48 downslope walking, combines the locomotion of backward walking and slope walking, 49 and is supposed to be a more challenging task on the neuromuscular system (Lay, 2005; 50 Lay et al., 2007). It is confirmed in physiological and biomechanical studies that, like 51 backward level walking, BSW could not only provide better cardiovascular function, 52 i.e. improved heart-rate, stroke-volume, cardiac output (Agbonlahor et al., 2009) and 53 greater demands on EMG activity, including increased level of muscle activity of 54 55 anterior tibialis during the entire gait cycle and of gastrocnemius between the phases of mid-swing to initial contact (Cipriani et al., 1995), but also facilitate gait balance, 56 meanwhile, minimize force related to injuries (Bates & McCaw, 1986). On the other 57 58 hand, compared to backward level walking, BSW has more advantages in exercising cardio-respiratory function and the lower extremity joints gradually and adequately by 59 adjusting the grade (Agbonlahor et al., 2009; Hoogkamer et al., 2014), as the motor 60 control system is predicted to require different walking strategies for slope walking 61 (Lay et al., 2006; Sheehan & Gottschall, 2012). Thus, BSW has become a popular 62 means of rehabilitation training for neurological impaired patients (Werner et al., 2002) 63 or patients with a weak knee extensor (Agbonlahor et al., 2009; Cipriani et al., 1995). 64 When BSW is used for rehabilitation purposes, it is conceivable that greater 65 challenges exist among the population with poor balance control ability, as high fall 66 incidence occurs during walking backwardly (Laufer, 2005) or walking on slopes 67 (Sheehan & Gottschall, 2012). The results of our previous investigation supported that 68

the task of backward walking did reduce the local dynamic stability of the locomotion 69 of lower extremity joints and trunk segment (Wu et al., 2015). Besides, the stability on 70 71 the lower limb joints (Sheehan & Gottschall, 2012) and the trunk segment (Cromwell, 2003; Leroux et al., 2002; Vieira et al., 2017a) were also found to be reduced during 72 73 upslope walking. To our knowledge, unfortunately, to date no study has reported gait stability during backward walking on inclined surfaces, leading to limited knowledge 74 on how the motor control system responds to the dual effect of walking direction and 75 slope grade. Thus, there is a need to evaluate gait stability during BSW in healthy 76 participants, which is a pre-requisite for its application on future research concerned 77 with pathological gait. 78

Gait variability measures are widely used in practice with proven success in 79 80 predicting the probability of falling (Bruijn et al., 2013; Dingwell & Marin, 2006). The 'variability' usually refers to the amount of variation of a kinematic parameter over 81 strides. It may quantify the spatial variation of stride, i.e. the magnitude of the variation. 82 83 The increased gait variability was believed to be a sign of poor gait stability, which means that the gait system is incapable of accurately achieving the desired goal (Vieira 84 et al., 2017b). The present study applied the local dynamic stability to reflect different 85 properties of the walking dynamics from gait variability. It may quantify the temporal 86 structure of stride variation. Unlike the gait variability that treats each gait cycle as 87 independent, the local dynamic stability evaluates the evolution of stability over several 88 strides (Vieira et al., 2017b). The local divergence exponent estimated from kinematic 89 data (, e.g. joint angles and segment velocities) during a steady-state walking trial is a 90

measure of local dynamic stability (Bruijn et al., 2013). It may quantify the sensitivity 91 of the neuromuscular system to small perturbations during continuous walking, by 92 93 characterizing how fast the neighboring trajectories of a reconstructed state space diverge after a small perturbation (Bruijn et al., 2012). The larger local divergence 94 exponents are corresponded to a poorer ability of balance recovery. The local 95 divergence exponent calculated from strides over a shorter period (one stride cycle, 96 labeled λ_s) is used to forecast the probability of falling during walking. The construct, 97 predictive and convergent validity of λ_s was found to be better supported in falling 98 prediction (Bruijn et al., 2013). 99

This study aimed to estimate the local dynamic stability of the locomotion of lower 100 extremity joints and trunk segment during backward upslope walking (BUW). Here, 101 102 we treated the measures of the trunk segment and lower extremity joints as independent 'locomotion systems', so as to obtain an exact state estimate of walking by numerical 103 methods. Therefore, we calculated the short-term local divergence exponents (λ_s) for 104 105 the joints and the segment. We then tested the effect of walking direction by comparing the stability during BUW with forward upslope walking (FUW) at the same grade; and 106 107 the effect of slope grade by comparing the stability at different grades during BUW and FUW, respectively. The mean standard deviation (MeanSD) was further quantified as 108 the amount of gait variability to provide more insight into the effect of walking direction 109 and slope grade on the gait stability (Lay, 2005; Lay et al., 2006; Leroux et al., 2002). 110 The gait stability was found to be challenged during backward walking (Wu et al., 2015) 111 and slope walking (Cromwell, 2003; Sheehan & Gottschall, 2012). Therefore, we 112

113	hypothesized that compared to FUW, the local dynamic stability and the stride-to-stride
114	gait variability of the lower extremity joint (, i.e. the hip, the knee and the ankle) angles
115	and the trunk segment velocity were worse during BUW (, i.e. λ_S and MeanSD for the
116	joint angles and segment velocity would be larger,) and would be further challenged by
117	the increasing grades.
118	
119	METHODS
120	Participants
121	Sixteen young adults (nine male, seven female; age 23.8 ± 1.4 years; height $1.69 \pm$
122	0.04m, BMI 20.46 \pm 2.50 kg/m ²) were recruited for the study. None of the participants
123	reported orthopedic or neurological injuries or disorders that could affect gait, and all
124	of them were capable of ambulating independently without any assistive device. The
125	experimental protocol was reviewed and approved by the Institutional Review Board
126	at Biomedical Engineering School of Shanghai Jiao Tong University and the informed
127	consent was obtained from each participant before the scheduled test date.
128	
129	Experimental Protocol
130	For familiarization, the participants were habituated to the walking area on a
131	treadmill (F80 Sole Fitness, Jonesboro, AR, USA) in a backward and forward upslope
132	way (BUW/FUW) at each of four grades (0%, 5%, 10%, 15%). The running surface of
133	the treadmill was 56 cm×152 cm in size with no force sensor installed. The participants

134 may practice each walking condition for 5 minutes with at least 5 minutes rest before

the data collection began. The tasks of downslope walking were not included in this 135 study. During pilot tests, most participants complained such tasks were too difficult, 136 and they were afraid of those tasks especially in a backward direction on a treadmill. 137 Thus, the participants were only allowed to walk upwards at gentle grades with their 138 preferred walking speed (PWS). The PWS in each walking direction at each grade was 139 determined following a previously reported protocol (Dingwell & Marin, 2006). During 140 the experiment, the participants completed a 5-min walking trial under each walking 141 direction at four grades with PWS. All participants were blinded to their exact walking 142 143 speeds throughout the experiment. These trials with different walking conditions were performed in a randomized order for each participant. The participants were asked not 144 to hold or touch the treadmill handles by hands or by other body parts during walking. 145 146 They were allowed a break of minimum 3 minutes between trials. An 8-camera motion capture system (Vicon T40, Oxford Metrics, Oxford, UK) 147 operating at 100 Hz was used to record the participants' body movement by capturing 148 149 the refined Cleveland Clinic Marker set including forty-two reflective markers placed on each participant. The four rigid clusters each consisted with four tracking markers 150 were respectively attached in the middle part of the thighs and shanks of both sides. 151 The anatomical markers were placed on the relevant locations of the lower extremity 152 153 joints and trunk landmarks. (Figure 1)

154

[Insert Figure 1]

155

156 Data Processing

Marker kinematics were low-pass filtered with a cut-off frequency of 10Hz using 157 a fourth-order and zero-lag Butterworth filter prior to data analysis. We included 100 158 consecutive strides for quantifying the local dynamic stability and gait variability based 159 on the angle of hip, knee and ankle joint in the motion of flexion-extension (FE), 160 abduction/adduction (AB/AD) and internal/external rotation (RT), as well as the linear 161 velocity of the trunk segment in the motion of anterior-posterior (AP), medial-lateral 162 (ML) and vertical (VT) (Figure 2 (a)). The angles were calculated by using Visual3D 163 software (v5 Professional, C-Motion Inc., USA). The linear motion of the trunk 164 165 segment was defined using a virtual center marker, defined as the average location of the four markers: *clavicle*, *sternum*, *7th cervical vertebrae*, and *10th thoracic vertebrae* 166 (Figure 1). The data of strides calculated during BUW and FUW both began and ended 167 168 at foot contact. Foot contact was identified as the intra-stride maximum of the heel marker in anterior-posterior (AP) direction during both FUW and BUW. 169

170

171 *Local Dynamic Stability*

The local dynamic stability of the above joint angles and trunk velocity was characterized by the local divergence exponents (λ_s). Time series were time-normalized to 10 thousand samples to eliminate the effect of time series length on the calculation of local divergence exponents (Bruijn et al., 2013) (**Figure 2 (b)**), using a shapepreserving interpolation predefined in MATLAB (Version R2012a, The MathWorks, Inc., USA). This interpolation is based on a cubic spline using not-a-knot end conditions. The interpolated value at a query point is based on a cubic interpolation of the values

at neighboring grid points. Meanwhile, the stride-to-stride temporal variations were 179 preserved by leaving the number of data points during each stride unnormalized. We 180 181 reconstructed a 5-dimensional state space from the time-normalized time-series using a constant delay of 10 samples (Figure 2 (c)). The embedding dimension was 182 determined by the global false-nearest-neighbor analysis, while the selected time delay 183 was estimated using the first minimum of the average mutual information function. The 184 local divergence exponents were calculated according to the algorithm described by 185 Rosenstein et al (Rosenstein et al., 1993). In the reconstructed state space, all pairs of 186 187 the nearest neighboring points were identified, and the Euclidean distances between the nearest neighbors were calculated and tracked until the end of the time series. A time 188 vs. the Euclidean distance curve representing the average logarithmic rate of Euclidean 189 190 distances (i.e. the divergence) over all original nearest neighbor pairs then can be obtained. The local divergence exponent was calculated as the slope of the curve. In 191 our study, we expressed the rate of divergence across the span of 0-0.5 stride, i.e. the 192 193 short-term divergence exponent, λ_{S} (Figure 2 (d)).

194

[Insert Figure 2]

195

196 Gait Variability

The stride-to-stride variability of the above joint angles and trunk velocity was determined by calculating the mean standard deviations (MeanSD). Data within the given strides were time-normalized into 101 samples (0–100%) per stride (**Figure 3** (a)). The standard deviation over the included 100 strides for each sample was

201	calculated (Figure 3 (b)). MeanSD was determined as the averaged value of the
202	standard deviations over all percent of the gait cycle.

[Insert Figure 3]

204

205 Statistical Analysis

The generalized estimating equations (GEE), a regression technique taking 206 repeated measures into account (Liang & Zeger, 1986), was used to determine the 207 significant effect of walking direction (with two levels: FUW and BUW) and slope 208 grade (with four levels: 0%, 5%, 10%, and 15%) on local dynamic stability and stride-209 to-stride variability. PWS of each participant was included during GEE as a covariate 210 to exclude the effect of walking speed. (the dependent variables: λ_s /MeanSD, 211 212 respectively, the covariate: PWS, and the independent variables: walking direction/slope grade). The homogeneity of regression slopes was tested by checking 213 the significance of the interaction between PWS and walking direction/slope grade, 214 respectively. The simple effect of direction within different grade conditions, as well as 215 the grade effect within different direction conditions would be checked respectively. 216 The effects of direction and grade on PWS and stride length were additionally checked 217 by two-way repeated measures ANOVA. All post hoc multiple comparisons were 218 219 performed using Bonferroni adjusted t tests. Linear regression analysis was used to test the relationship between PWS and λ_s , as well as between PWS and MeanSD, 220 221 respectively. The relationship between the λ_S and the MeanSD was also tested by the same analysis. Significant level p of all tests was chosen as .050. All data were 222

223	processed by SPSS Statistics software (Version 17.0, SPSS Inc., USA).
224	
225	RESULTS
226	PWS and Stride Length during BUW
227	The PWS was significantly affected by the walking direction ($p < .050$). Compared
228	to FUW, a smaller PWS was found during BUW at each grade (Table 1). As for the
229	effect of slope grade, the PWS during both FUW and BUW at steeper grades were
230	smaller than at gentler ones ($p < .050$, respectively). There was no walking direction
231	effect on stride length ($p > .050$), while significant grade-related differences existed in
232	both BUW and FUW conditions ($p < .010$, respectively). Smaller stride length was
233	observed at steeper grades during both BUW and FUW. No interaction between
234	directions and grades existed in PWS and stride length ($p > .100$, respectively).
235	[Insert Table 1]
236	
237	Local Dynamic Stability during BUW
238	Effects of Walking Direction on λ_s
239	λ_s for the lower extremity joint angles and the trunk velocity were significantly
240	affected by the walking direction (Figure 4 and Table 2). Compared to FUW, larger λ_s
241	for the knee AB/AD angle at 0%, 5% grades and the ankle AB/AD angle at all grades
242	displayed during BUW ($p < .050$, respectively). Significant larger λ_S was also shown in
243	RT angle of all joints and in the trunk VT velocity during backward level walking than
244	during the forward condition ($p < .050$), respectively. An exception was the hip FE

angle, where significant smaller λ_s was found during BUW at 10% and 15% grades (*p* < .050, respectively).

247

248 Effects of Slope Grade on λ_S

For lower extremity joint angles, no grade effect on λ_s existed during BUW 249 (p > .010) (Figure 4). Meanwhile, λ_s for all joint angles increased with the growing 250 grades during FUW. In all motion directions, λ_S for the hip angles at 0% and 5% grade 251 were significantly smaller than at steeper grades during FUW (p < .050, respectively). 252 Similarly, the knee and ankle angles during FUW displayed smaller λ_s at 0%, 5% grade 253 than at 15% grade (p < .050, respectively). λ_s for the trunk velocity significantly 254 increased with the growing grades during FUW and BUW. In both walking directions, 255 256 the trunk ML velocity displayed smaller λ_s at 0%, 5% grade than at 15% grade, while pairwise difference among all four grades were significant in the VT velocity that a 257 smaller λ_S was observed at the gentler grade (p < .050, respectively). No interaction was 258 259 found between walking directions and slope grades in λ_s (p > .050) (Table 2).

260

[Insert Figure 4]

261

[Insert Table 2]

262

263 Gait Variability during BUW

264 Effects of Walking Direction on MeanSD

For different joint angles, the effects of walking direction on MeanSD were variously presented (**Figure 5**). The MeanSD for the hip FE angle and the knee FE, AB/AD angle during BUW were smaller than during FUW at 10% and 15% grade (p<0.050, respectively). Significantly larger MeanSD were found in ankle joint angle at all grades during BUW than during FUW (p < .050, respectively). As to the trunk velocity, compared to FUW, the MeanSD during backward level walking were larger in all motion directions (p < .050, respectively).

272

273 *Effects of Slope Grade on MeanSD*

There were significant interaction effects on MeanSD between walking directions 274 and slope grades in the hip and knee FE angles (p < .050, respectively) (Figure 5). 275 During FUW, the MeanSD for these two joint angles at 10% and 15% grade were larger 276 than those at gentler grades, while the grade effects were just the opposite during BUW 277 (p < .050, respectively). Compared to gentler grades, significantly larger MeanSD at 278 10% and 15% grade were also found in the knee AB/AD joint angle during FUW (p 279 <.050, respectively). No grade related difference was found in the RT angle of any joint 280 during either BUW or FUW (p > .050). As to the trunk velocity, the grade effect only 281 existed during FUW. The MeanSD in AP and ML motion during forward level walking 282 were significantly smaller than during slope, while significant pairwise difference 283 existed among almost all grades in the VT velocity that a smaller MeanSD was observed 284 at the gentler grade (p < .050, respectively). 285

286

[Insert Figure 5]

287

288 Relationship between PWS and λ_S / MeanSD

289	For both walking directions, PWS showed a significant negative relationship with
290	λ_s in all motion directions of the joint angles and the trunk velocity ($p < .001$,
291	respectively). (Table 3) The relationship between PWS and λ_S for the trunk segment in
292	AP direction of a particular participant was further displayed as scatterplots. (Appendix
293	Figure)
294	[Insert Table 3]
295	
296	Whether during FUW or BUW, there was no significant relationship between PWS
297	and MeanSD in any motion direction of the joint angles and the trunk velocity ($p > .100$,
298	respectively). (Table 4)
299	[Insert Table 4]
300	
301	Relationship between λ_s and MeanSD
302	During BUW, λ_s showed a significant negative relationship with the MeanSD in
303	all motion directions of the lower extremity joint angles, and the trunk velocity in AP
304	motion as well ($p < .010$, respectively). Positive correlations were found in all motion
305	directions of both lower extremity joint angles and the trunk velocity ($p < .010$,
306	respectively) during FUW, except for the RT angle of the lower extremities ($p = .070$)
307	(Table 5).
308	[Insert Table 5]
309	
310	DISCUSSION

In our previous investigation, compared to forward walking, gait stability during 311 backward walking was shown to be challenged (Wu et al., 2015). On the other hand, 312 313 walking on the inclined surfaces was also found to decrease local dynamic stability particularly in upslope conditions (Vieira et al., 2017a). Unfortunately, as far as we 314 315 knew, to date no study has reported gait stability during backward walking on inclined surfaces. This was the first time that the dual effects of the walking direction and slope 316 grade on the gait stability of the joint and segment motions were investigated, aiming 317 to predict whether the gait stability would be challenged during BUW, so as to examine 318 319 whether BUW would be a promising tool to train gait stability.

It was consistent with the original hypothesis that, backward walking did 320 negatively influence the local dynamic stability of the human locomotion on inclined 321 322 surface. This may be explained by the fact that during backward walking, the subject lacks the visual information to process, and fears bumping and falling because 323 backward walking is not habitually performed (Nadeau et al., 2003). Consequently, 324 compared to walking forwards, a reduced walking speed (, which was validated in the 325 present study,) and a greater effort were required for the neuromuscular system to 326 control lateral oscillations of the body when walking backwards (Nadeau et al., 2003). 327 In our study, this effect of walking direction was especially significant for the AB/AD 328 angles of the knee and ankle joint, as these joints showed worse local dynamic stability 329 during backward walking. Our previous unpublished results on the total range of motion 330 showed that values of the knee and ankle AB/AD angle during BUW were significantly 331 smaller compared to FUW (p < .050, respectively). (See Appendix Table) This postural 332

adaption may induced by the greater control imposed on the knee and ankle joint 333 demonstrated by increased muscle activity (Katsavelis et al., 2010), so as to overcome 334 335 the worse stability of the joint motion and avoid falls during BUW. In our study, compared to BUW, a reduced local dynamic stability in hip FE angle was identified 336 during FUW. We speculated the hip joint during FUW needed to expend more control 337 effort to stabilize its motion, which was similar to the kinetic demands for knee joint 338 during BUW. These results could be supported by Lay et.al that (Lay, 2005), a larger 339 moment and higher power in the hip FE joint motion were found during FUW in 340 341 comparison with BUW, while the opposite effect of walking direction was observed on the kinetic data of the knee joint. Backward walking direction did little impact on the 342 stability of the trunk motion in the present study. This might be due to the stabilization 343 344 strategy adopted by the trunk segment, that during backward walking the trunk was supposed to adopt a generally rigid functioning with (, i.e. rigidly linked to) the 345 underlying supporting segment in both sagittal and frontal plane (Nadeau et al., 2003). 346 347 Our results thus further prove the effectiveness of the trunk stabilization strategy during BUW. 348

The effect of the slope grade on the local dynamic stability of the lower extremity joint motion was significant during FUW, where the stability of all joints reduced as the grade increased. This was mostly concordant with the grade-related difference in MeanSD of FE and AB/AD motion, which was further supported by the positive correlation between λ_s and MeanSD during FUW. Results in previous studies were consistent with ours as well, that in comparison with level walking, (forward) slope

walking would reduce the gait stability in both sagittal and frontal plane, thus resulting 355 in a greater fall risk (Gottschall & Nichols, 2011; Sheehan & Gottschall, 2012). These 356 357 results indicate that the active control is required to stabilize the lower extremity joints in all motion directions during slope walking. In order to raise the center of mass (COM) 358 and prevent falling on the inclined surfaces, the motor control system needs to handle 359 the altered vertical foot displacement and its clearance, as well as the higher horizontal 360 friction demands compared to the level walking (McIntosh et al., 2006). All these 361 changes of walking pattern may explain the observed effect of slope grade on the gait 362 stability of the lower extremity joints. Meanwhile, for BUW conditions, there was no 363 grade-related difference in λ_s for any joint. In our study, significant negative 364 correlations between λ_S and MeanSD were found in all angular motions during BUW, 365 366 indicating that these two metrics responded oppositely to the changes of the slope grade under backward walking conditions. For example, the gait variability (indicated by the 367 value of MeanSD) of the knee joint even attenuated with the increasing grades during 368 369 BUW, while the local dynamic instability (indicated by the value of λ_s) slightly increased. These results further supported that measurements of local dynamic stability 370 and gait variability quantify fundamentally different properties of walking dynamic 371 (Dingwell & Marin, 2006; Vieira et al., 2017a). Here, a possible interpretation is that, 372 to accommodate BUW, a demanding walking task that accompany backward direction 373 and inclined surface, the motor control system may reduce and control the gait 374 variability (, i.e. the spatial variation of consecutive strides) of the knee joint angle, in 375 exchange for its moderate increasing local dynamic instability (i.e. with no 376

significantly-changed temporal structure of stride variation) (Dingwell & Marin, 2006). 377 The local dynamic stability of the trunk motion was quite sensitive to grade-related 378 differences. A challenged stability of the trunk ML and VT motion was found at the 379 steeper inclined surface under both FUW and BUW conditions. It supported the finding 380 by Kang et al., that the trunk motion is a more sensitive marker of impaired gait function 381 compared to lower extremity joints (Kang & Dingwell, 2009). The gait stability in 382 medial-lateral direction is important for controlling body balance and predicting falls 383 (Bauby & Kuo, 2000; Maki & Mcilroy, 2006), therefore our results indicated that 384 385 compared to level walking, upslope walking may impose more challenges on the gait stability in both forward and backward walking direction in an effective way. 386 Furthermore, our finding was well consistent with the previous study on FUW (Vieira 387 388 et al., 2017a), that our measurements of the local dynamic stability and gait variability showed a similar trend with the increasing grades. Still, since the trunk stability 389 displayed no significant direction-related difference, there was no extra challenge on 390 the trunk stability during BUW compared to FUW. 391

Additionally, we found no significant interaction effect on λ_s . Therefore, we consider that upslope walking in both directions may be promoting tools to train local dynamic stability, as the expected performance of the rehabilitation can be achieved by setting customized grades of the walking surface. Moreover, BUW under safe conditions (, e.g. with harness) may be an alternative advanced strategy for future training on gait stability. It may show improvements for the stability of both upper and lower body motion (, e.g. for elderly), which remains to be shown during normalwalking.

400 There were several limitations in this study. The healthy young participants walked at a relatively lower speed on the treadmill. We attribute it to the fact that these 401 participants walked barefoot on treadmill, so that their foot motion can be tracked more 402 accurately. Another fact is that, no safety harness was applied for our participants, 403 which made them a bit worry and slow down during the experiment. To exclude the 404 effect of walking speed indicated by Table 3 and Table 4, in present study, PWS was 405 406 considered as a covariate during the statistical analysis. Additionally, the participants were asked to walk upward on the treadmill at gentle grades, as this walking condition 407 is a safer and more common activity of daily living. Still, walking on steeper slopes 408 409 may be used as a perturbation of normal locomotion (Lay, 2005; Lay et al., 2007), so that the capacity of the joint/segment to recover from this perturbation can be further 410 investigated. When safety is secured (, e.g. with a harness), the downward slope walking 411 412 should also be investigated in future work to provide more insight into its gait stability, and can be considered as a promising training condition as well. More pre-experiment 413 trainings may help the participants overcome not only the difficulties in practical 414 experience but also the fear of falling. Furthermore, a larger study could be proposed 415 to examine whether applying speed constrains during training may provide a challenge 416 for gait stability among the elderly or patients during BSW as the BSW is frequently 417 418 prescribed for those specific populations as a rehabilitation treatment.

CONCLUSIONS

421	The local dynamic stability of the human locomotion during upslope walking was
422	challenged by the backward walking direction or increasing slope grades. As for BUW,
423	the backward walking direction challenged the local dynamic stability of the motion of
424	lower extremity joints, while the increasing grade imposed large challenges on the
425	stability of the trunk motion. Therefore, BUW can be considered as a training tool for
426	the stability of both upper and lower body motion during gait.
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Tables

		FUW			BUW				
	0%	5%	10%	15%	0%	5%	10%	15%	
PWS (m/s)	0.73	0.72	0.71	0.71	0.49	0.47	0.47	0.47	
	(0.10)	(0.09)	$(0.07)^{a}$	$(0.08)^{b}$	(0.05) ^{#,c}	$(0.05)^{\#}$	(0.09)#	$(0.06)^{\#}$	
Stride	0.83	0.81	0.75	0.74	0.80	0.79	0.77	0.74	
length (m)	(0.17)	(0.16)	(0.12) ^a	(0.13) ^b	(0.11)	(0.13)	(0.12)	$(0.12)^{d}$	

498 .050 for FUW compared to BUW within the grade condition p $^{a}p < .050$ for 0%, 5% grade compared to 10% grade within the direction condition 499 ^{b}p < .050 for 0%, 5% grade compared to 15% grade within the direction condition 500

 ^{c}p < .050 for 0% grade compared to 5%, 10% and 15% grade within the direction 501 condition 502

 ^{d}p < .050 for 0%, 5% and 10% grade compared to 15% grade within the direction 503 condition 504

505

Table 2 Results of statistical analysis for the effect of walking direction/slope grade on 506 λs

507

		Effect of walking		Effect o	f slope	Interaction		
		direction		gra	de	effec	t	
		<i>F</i> (1, 15)	р	F(3, 45)	р	F(3, 45)	р	
	FE Angle	5.01	.026*	3.39	.020*	2.11	.102	
Hip	AB/AD Angle	0.79	.370	5.75	.001*	0.69	.560	
	RT Angle	4.68	.047*	6.87	<.001*	1.19	.315	
	FE Angle	3.28	.064	2.99	.043*	0.99	.398	
Knee	AB/AD Angle	9.13	.009*	5.97	<.001*	2.48	.064	
	RT Angle	7.12	.015*	5.58	.002*	0.56	.642	
	FE Angle	3.81	.053	1.89	.138	0.15	.928	
Ankle	AB/AD Angle	16.47	.001*	2.89	.048*	0.72	.544	
	RT Angle	6.23	.024*	2.87	.049*	1.58	.198	
	AP Velocity	2.05	.147	2.96	.044*	0.26	.851	
Trunk	ML Velocity	0.58	.446	4.28	.006*	0.05	.985	
	VT Velocity	5.30	.033*	16.55	<.001*	0.67	.571	

*p < .050 was set as significant level 508

			λ_S			
		-	a	b	р	
			(s.e.)	(s.e.)	<u> </u>	
		FE angle	3.560	-1.719	<.001*	
		I L ungio	(0.123)	(0.154)		
	Lower	AB/AD angle	3.251	-1.717	< 001*	
	extremity joints		(0.133)	(0.166)	.001	
		RT angle	2.645	-1.416	< 001	
PWS during		KI aligic	(0.124)	(0.156)	<.001*	
FUW (m/s)		A D volocity	3.774	-1.850	<.001*	
		Ar velocity	(0.169)	(0.211)		
	Tanalr	ML velocity	3.169	-1.458	<.001*	
	Irunk		(0.238)	(0.298)		
		VT velocity	2.970	-1.445	<.001*	
			(0.209)	(0.263)		
		FE angle	3.578	-1.753	<.001*	
			(0.149)	(0.191)		
	Lower		3.358	-1.695	<.001*	
	extremity joints	AB/AD angle	(0.130)	(0.166)		
	• •		3.088	-1.466		
PWS during		KI angle	(0.173)	(0.221)	<.001'	
BUW (m/s)			3.889	-1.815		
		AP velocity	(0.292)	(0.367)	<.001'	
	T 1		3.670	-1.524		
	Trunk	ML velocity	(0.261)	(0.334)	<.001'	
			2.899	-1.310		
		VT velocity	(0.252)	(0.322)	<.001*	

510	Table 3 Relationship between PWS and λ_s with the intercept (a), regression coefficients
511	(b) and their standard errors (s.e.)

512 The models used was $\lambda_S = a + b \times PWS$

* Significant relationship between walking speed and local dynamic stability (p < .050)

			MeanSD (Deg or m/s)		
			а	b	
			(s.e.)	(s.e.)	p
		EE angla	2.133	0.253	220
		FE angle	(0.539)	(0.800)	.329
	Lower	AB/AD angle	1.276	0.122	721
	extremity joints	AD/AD aligic	(0.282)	(0.354)	./51
		RT angle	1.171	0.205	.134
PWS during		KI aligic	(0.643)	(0.257)	
FUW (m/s)		AP velocity	3.144	1.207	.267
		AI velocity	(0.857)	(1.076)	
	Trunk	MI velocity	2.166	1.300	.146
	(×10 ⁻²)	WIL velocity	(0.683)	(0.879)	.128
		VT velocity	1.983	1.257	
			(0.643)	(0.811)	
		FE angle	2.918	0.677	508
			(1.002)	(1.283)	.398
	Lower	AB/AD angle	1.146	0.515	.473 .024
	extremity joints		(0.559)	(0.716)	
		RT angle	1.298	0.685	
PWS during		KI aligic	(0.232)	(0.301)	
BUW (m/s)		AP velocity	3.728	1.380	247
		In verservy	(0.918)	(1.176)	·27/
	Trunk	ML velocity	2.010	1.360	155
	(×10 ⁻²)	will velocity	(0.725)	(0.939)	.155
		VT velocity	1.562	1.487	207
		v i velocity	(0.891)	(1.161)	.207

515	Table 4 Relationship between PWS and MeanSD with the intercept (a), regression
516	coefficients (b) and their standard errors (s.e.)

517 The models used was MeanSD = $a + b \times PWC$

* Significant relationship between walking speed and gait variability (p < .050)

		_		MeanSD	
		-	a	b	р
			(s.e.)	(s.e.)	
		FE angle	2.064	0.687	<.001*
	Lower		(0.847)	(0.227)	
	extremity	AB/AD angle	2.085	0.374	.003*
	joints		(0.245)	(0.126)	
2	(Deg)	RT angle	2.401	-0.397	.070
As during			(0.210)	(0.112)	
		AP velocity	6.769	0.809	<.001*
ГUW			(1.136)	(0.372)	
	Trunk	ML velocity	2.609	0.246	.004*
	$(m/s \times 10^{-2})$		(1.294)	(0.081)	
		VT velocity	0.628	1.323	.006*
			(0.092)	(0.460)	
		FE angle	6.358	-1.317	<.001*
	Lower		(0.882)	(0.392)	
	extremity	AB/AD angle	2.929	-0.658	.006*
	joints		(0.486)	(0.234)	
2	(Deg)	RT angle	2.499	-0.317	.002*
As duning			(0.201)	(0.101)	
		AP velocity	12.153	-2.431	<.001*
DUW			(1.716)	(0.691)	
	Trunk	ML velocity	7.255	-1.763	.092
	$(m/s \times 10^{-2})$		(0.885)	(0.383)	
		VT velocity	6.436	-1.647	.664
			(1.150)	(0.551)	

520	Table 5 Relationship between λ_S	and MeanSI	O with the intercept	ot (a) , regression
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521 coefficients (b) and their standard errors (s.e.)

522 The models used was MeanSD = $a + b \times \lambda_S$

523 * Significant relationship between local dynamic stability and gait variability (p < .050)

525	Figure Captions
526	Figure 1 — Illustration in all views of marker displacement
527	
528	Figure 2 — Examples of a representative set of hip flexion-extension (FE) angle data.
529	(a) Original time-series within 100 strides in 15570 seconds; (b) Normalized time-series
530	within 100 strides into 10 thousands samples; (c) Normalized data embedded in a 3D
531	state space (with time delay, i.e. τ of 10, and the real embedding dimension of 5), and
532	(d) Average logarithmic divergence vs. stride. The best fit linear slope of the logarithmic
533	relation from 0 to 0.5 stride represents λ_s .
534	
535	Figure 3 — Examples of a set of hip flexion-extension (FE) angle data across the
536	normalized stride duration. (a) Normalized time-series of 100 separate strides, and (b)
537	Mean (solid line) \pm SD (dash lines) for data shown in (a).
538	
539	Figure 4 — The effects of the walking direction and slope grade on λ_S for the (a) FE,
540	(b) AB/AD, and (c) RT motion of the lower extremity joints, and (a) AP, (b) ML, and (c)
541	VT motion of the trunk (# indicates significant direction effect, while * indicates
542	significant grade effect, $p < .050$, respectively)
543	
544	Figure 5 — The effects of the walking direction and slope grade on MeanSD for the (a)
545	FE, (b) AB/AD, and (c) RT motion of the lower extremity joints, and (a) AP, (b) ML,
546	and (c) VT motion of the trunk (# indicates significant direction effect, while * indicates

547 significant grade effect, p < .050, respectively)

Appendix

550 Appendix Table The effects of the walking direction and slope grade on the total range 551 of motion of the lower extremity joints, mean (SD)

#17 <		Total ran	ge of mot (deg	ion durir g)	ıg FUW	Total ra	nge of mc (d	otion duri eg)	ng BUW
050 £		0%0	5%	10%	15%	0%0	5%	10%	15%
	FE Angle	35.99 (6.26)	38.34 (5.83) ^e	40.07 (5.50) ^a	42.77 (5.03) ^d	30.37 (6.69)#	27.71 (6.03)#,e	23.82 (7.15)#,ª	19.86 (6.50)#,d
Hip	AB/AD Angle	8.07 (1.91)	8.38 (1.58)	8.36 (1.26)	8.09 (0.99)	5.87 (1.43)#	6.25 (1.75)#	6.75 (1.80)#	6.33 (1.60)#
	RT Angle	14.12 (3.30)	14.58 (3.165)	14.61 (3.06)	13.96 (2.95)	9.85 (3.14)#	9.26 (2.89)#	9.37 (2.46)#	8.55 (1.97)#,d
7 within 4	FE Angle	60.44 (9.78)	59.60 (8.72)	59.59 (9.04)	61.07 (9.47)	51.12 (11.61)#	51.51 (10.81)#	52.28 (11.20)#	53.03 (8.98)#
knee	AB/AD Angle	10.63 (4.04)	11.15 (3.93)	12.87 (4.20) ^a	13.02 (3.94) ^b	8.64 (3.53)#	8.18 (3.13)#	7.62 (3.16)#	7.96 (3.00)#
aanditia	RT Angle	15.22 (2.80)	14.34 (3.18)	13.79 (3.07)°	12.87 (2.89) ^b	13.05 (3.79)#	12.29 (3.61)#	11.97 (3.87) ^c	11.37 (3.87) ^b
	FE Angle	17.49 (4.09)	16.93 (5.01)	17.90 (5.52)	19.04 (6.03)	25.23 (4.39)#	28.01 (5.63)#,e	30.64 (5.41) ^{#,a}	32.12 (5.75)#,d
Ankle	AB/AD Angle	18.56 (3.18)	18.63 (3.71)	18.87 (4.04)	19.27 (4.24)	13.26 (2.77)#	13.00 (3.32)#	12.56 (3.23)#	12.44 (2.89)#
	RT Angle	10.41 (2.83)	10.67 (3.73)	10.64 (3.47)	10.30 (3.16)	10.45 (3.23)	10.69 (3.01)	11.61 (2.95) ^a	11.64 (2.75) ^b

⁵⁵² p < .050 for FUW compared to BUW within the grade condition ⁵⁵³ p < .010 for 0%, 5% grade compared to 10% incline within the direction condition ⁵⁵⁴ p < .050 for 0%, 5% grade compared to 15% incline within the direction condition

p < .050 for 0% grade compared to 10% incline within the direction condition

556 ^{d}p <.050 for 0%, 5%, 10% grade compared to 15% incline within the direction condition

557 $^{\text{e}}p < .050$ for 0% grade compared to 5% incline within the direction condition

549

[Insert Appendix Figure]

560 Appendix Figure — Scatterplots of λ_S against PWS for each of (a) the walking 561 direction conditions, and (b) the slope grade conditions, for the trunk segment in 562 anterior-posterior (AP) direction. Each symbol representing the λ_S of a particular 563 participant. Lines with different dash types are the linear regression slopes for the 564 particular condition.

Figures



566

Figure 1



Figure 2



571

Figure 3







Figure 4







Figure 5

Appendix Figure

(b)

1.20



